## **Detailed Solutions**



Evening Session

1st March, 2014





India's Best Institute for IES, GATE & PSUs

# **Expert Opinion**



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ear Students,
The Questions of GATE 2014: EE are based on fundamental and basic concepts of the syllabus. There is no ambiguity and misprint noticed till now, however, it is an observation based on students feedback.

The level and standard of GATE 2014 questions are almost similar to the exam of GATE 2013. There are 3 important observations made by me about GATE 2014 exam.

1. The GATE exam 2014 has been conducted in 4 seatings. The questions were different in each session but difficulty level of questions were almost equal. The standard of the questions were quite average, however it varies on the perception of person to person also.

The average marks on all the papers should be equated and necessary scaling criteria should be adopted for this purpose.

2. The GATE 2014 cut off is expected to be slightly higher than previous year. The cut-off may vary between 27-30 marks (General Category).

GATE Cutoff = Total Marks obtained by all the candidates

Total number of candidates

3. In my opinion the toppers marks of GATE-2014 would be between 85 to 90 marks.

Note

If you have more questions (except from this paper) of GATE 2014: EE, then kindly mail it to: <a href="mailto:madeeeasydelhi@gmail.com">madeeeasydelhi@gmail.com</a>

Note: Please do mention name, mobile no, date & session of exam, while sending the mail. You may also submit directly (in handwritten format) at MADE EASY Kalu Sarai Office.

Disclaimer

Dear Students, MADE EASY has taken due care in collecting the data and questions. Since questions are submitted by students and are memory based, therefore the chances of error can not be ruled out. Therefore MADE EASY takes no responsibility for the errors which might have incurred.

# Super **Talent Batches**



India's Best Institute for IES. GATE & PSUs

# Electrical Engineering Super Talent Batches at Delhi Centre 1 st Batch: Commencing from 2nd June Morning Batch 2 nd Batch: Commencing from 25th June Evening Batch

Eligibility (Any of the following)

- Top 2000 Rank in GATE
- B.Tech from IIT
- Appeared in IES or 3 PSUs Interview
- B.Tech from NIT with 65% marks
- B.Tech from Private Engineering college with 70% marks

**Benefits** 

- **Better Teaching Environment**
- Extra teaching hours
- In-depth coverage of subjects

### **Gate 1st March Evening**

**Q.1** If 
$$\left(z + \frac{1}{z}\right)^2 = 98$$
 then the value of  $\left(z^2 + \frac{1}{z^2}\right) = ?$ 

Solution: (96)

$$\left(z + \frac{1}{z}\right)^2 = 98$$

$$\Rightarrow \qquad z^2 + \frac{1}{z^2} + 2 = 98$$

$$\Rightarrow \qquad \qquad z^2 + \frac{1}{z^2} = 96$$

Q.2 Choose the most appropriate word from the option given below to complete the following sentence:

He could not understand the judges awarding him the first prize, because he thought that his performance was quite

(a) Superb

(b) Medium

(c) Mediocre

(d) Exhilarating

Solution: (c)

**Q.3** Choose the closest meaning:

It is fascinating to see life forms COPE WITH varied environmental conditions.

(a) Adopt to

(b) Adapt to

(c) Adept to

(d) Accept with

Solution: (b)

Q.4 The Palaghat in southern parts are low lying areas with hilly terrain due to which parts of Tamil Nadu suffer rainfall and of Kerala suffer summer what it is conclude.

Being covered by upper and lower hilly regions

- (a) The Palaghat is formed due the upper hilly acts of Southern and Western India
- (b) The parts of Tamil Nadue and Kerala suffer season charges due to it
- (c) Monsoon are caused due to Southern disturbance
- (d) Tamil Nadu receives maximum rainfall due to it

Solution: (b)



Q.5 Scientists are now able to found the main root cause of depression and other Physiatric diseases with genetics main root cause.

In near future they will be able to provide cure for such diseases. What does it infer.

- (a) Depression and other diseases are caused due to genes
- (b) There is a cure for such diseases
- (c) Genes are main cause of all illnesses
- (d) Gene therapy will provide cure of all diseases

### Solution: (a)

Q.6 There is discount of 10% on total fare for a round trip and for group of 4 and more, there is 5% discount on total fare. If one way single person fare is Rs. 100. Find the group of 5 tourist round trip fare?

### Solution: (Rs.850)

Total round trip fare for group of 5 tourist without discount

$$= 5 \times 200 = \text{Rs.} 1000$$

- (i) Discount for round trip =  $\frac{10}{100} \times 1000 = \text{Rs.} 100$
- (ii) Discount for having of group of 5 tourist =  $\frac{5}{100} \times 1000 = \text{Rs.} 50$
- Total discount = Rs. 150
- ⇒ Total round trip fare for group of 5 tourist after discount

Q.7 The Minister speaks in a press conference after scam, minister said "The buck stops here", what he convey by this?

Choose the appropriate meaning of the given phrase.

- (a) He wants all the money
- (b) He will return the money
- (c) He will assume final responsibility
- (d) He will resist all enquries

### Solution: (c)

Q.8 In a survey 300 respondents were asked wheter they own a vehicle or not. If yes, they were further asked to mention whether they own a car or scooter or both. Their responses are tabulated below. What percent of respondents do not own a scooter.

		Men	Women
Owns	Car	40	34
	Scooter	30	20
	Both	60	46
Do not Owns		20	50

Solution: (48%)

Percent of respondents who do not own a scooter

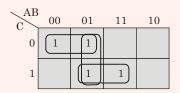
$$= \frac{74 + 70}{300} \times 100 = \frac{144}{300} \times 100 = 48\%$$

Find the logic circuit for the given K-map.

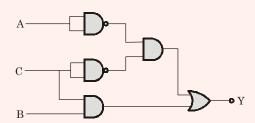
AB	00	01	11	10
0	1	1		
1		1	1	

[Note: Options are not available]

Solution:



$$Y = \overline{C} \overline{A} + CB + \overline{A}B$$



**Q.10** If  $X(s) = \frac{3s+5}{s^2+10s+21}$  is Laplace transform of x(t), then  $x(0^+)$  is

(a) 0

(b) 3

(c) 5

(d) 21

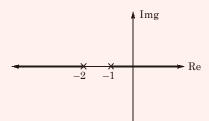
Solution: (b)

$$X(s) = \frac{3s + 5}{s^2 + 10s + 21}$$

$$\therefore \qquad \qquad x(0^+) = \lim_{s \to \infty} s \left( \frac{3s+5}{s^2+10s+21} \right)$$

$$= \lim_{s \to \infty} \left( \frac{3 + \frac{5}{s}}{1 + \frac{10}{s} + \frac{21}{s^2}} \right) = 3$$

Q.11 Root locus of unity feedback system is shown in figure.



Find closed loop transfer function.

(a) 
$$\frac{K}{(s+1)(s+2)}$$

(b) 
$$\frac{-K}{(s+1)(s+2)+K}$$

$$\text{(c)}\quad \frac{-K}{\left(s+1\right)\left(s+2\right)-K}$$

(d) 
$$\frac{K}{(s+1)(s+2)+K}$$

Solution: (c)

This is converse root locus of

$$G(s) H(s) = \frac{-K}{(s+1)(s+2)}$$

From given transfer function

From option (c)

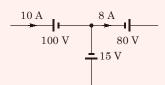
$$\frac{C(s)}{R(s)} = \frac{-K}{(s+1)(s+2) - K}$$

$$G(s) H(s) = \frac{-K}{(s+1)(s+2) - K - (-K)}$$

$$= \frac{-K}{(s+1)(s+2) - K + K}$$

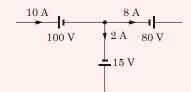
$$G(s) H(s) = \frac{-K}{(s+1)(s+2)}$$

Q.12 Total power absorbed by the given circuit is



Solution: (330 W)

Using KCL,



.. Total power absorbed = 
$$10 \times 1000 - [(80 \times 8) + (15 \times 2)]$$
  
=  $1000 - 640 - 30$   
=  $330 \text{ W}$ 

- Q.13 In a balance 3-phase system, 2 wattmeter method is used to measure the power. If reading of one wattmeter is twice of other, the load impedance angle (in radian) is

Solution: (c)

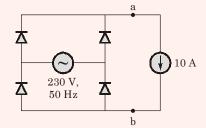
$$\tan \phi = \sqrt{3} \left[ \frac{W_1 - W_2}{W_1 + W_2} \right]$$
 [By two wattmeter method]

As 
$$W_1 = 2W_2$$
 [Given]

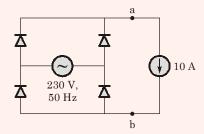
$$\tan \phi = \sqrt{3} \left[ \frac{2W_2 - W_2}{2W_2 + W_2} \right] = \frac{\sqrt{3}}{3} = \frac{1}{\sqrt{3}}$$

$$\Rightarrow \phi = \frac{\pi}{6} \text{ rad.}$$

Q.14 If current source is replaced by resistance R then find the value of R, to maintain same current through branch ab.



Solution:  $(23 \Omega)$ 



$$V_{ab} = 230 V$$

$$I_{ab} = 10 A$$

$$R_{ab} = \frac{V_{ab}}{I_{ab}} = \frac{230}{10} = 23 \Omega$$

Q.15 Cascade of three modulus-5 counters results in overall modulus of

(a) 5

(b) 25

(c) 125

(d) 625

### Solution: (c)

Overall modulus of cascade of three modulus-5 counters =  $5 \times 5 \times 5 = 125$ .

Q.16 For a 400 V, 50 Hz, 4 pole, Y-connected alternator.

 $OCC: V_{OC} = 400 V(rms, line to line), at I_f = 2.5 A.$ 

 $SCC: I_{SC} = 10 A \text{ (rms, phase)}, at I_f = 1.5 A.$ 

Find per phase synchronous impedance in ohm at rated voltage.

Solution:  $(13.85 \Omega)$ 

$$V_{OC_{L-L}} = 400 \,\mathrm{V}$$

$$\label{eq:Voc_ph} \begin{array}{ll} : : & V_{\rm OC_{ph}} \; = \; \frac{400}{\sqrt{3}} \; V \bigg|_{I_f \; = \; 2.5 \; \rm A} \end{array}$$

$$I_{SC_{ph}} = 10 A|_{I_{f} = 1.5 A}$$

$$... \hspace{1.5cm} I'_{\rm SC_{\,ph}} \; = \; \frac{10}{1.5} \times 2.5 = \frac{50}{3} \; A \bigg|_{I_{\rm f} \; = \; 2.5 \; A}$$

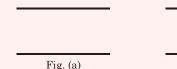
[: of linear relationship between  $I_{sc}$  and  $I_{f}$ ]

Per phase synchronous impedance

$$= \left. \frac{V_{OC_{ph}}}{I'_{SC_{ph}}} \right|_{I_f = 2.5 \text{ A}}$$

$$= \frac{400/\sqrt{3}}{50/3} = 13.85 \,\Omega$$

 $\mathbf{Q.17}~\mathrm{C_o}$  is capacitance of parallel plate capacitor with air as dielectric. When half of gap is filled with dielectric of permittivity  $\in_{\mathbf{r}}$  then modified capacitance is



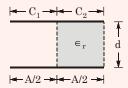
(a) 
$$\frac{C_o}{2}(1+\epsilon_r)$$

(b) 
$$C_o \in r$$

(c) 
$$\frac{C_o}{2} \in_r$$

(d) 
$$C_o(1+ \epsilon_r)$$

Solution: (a)



As 
$$C_o = \frac{A \in_o}{d}$$

where,

A = Area of the parallel plate capacitor

d = Distance between the plates

$$\therefore \qquad C_1 = \frac{\frac{A}{2} \epsilon_0}{d} \text{ and } C_2 = \frac{\frac{A}{2} \epsilon_0 \epsilon_r}{d}$$

As both  $\boldsymbol{C}_1$  and  $\boldsymbol{C}_2$  are in parallel

$$\therefore \qquad C_{\text{net}} = C_1 + C_2$$

$$= \frac{A \in_0}{2d} + \frac{A \in_0 \in_r}{2d}$$

$$= \frac{A \in_0}{2d} + \frac{A \in_0 \in_r}{2d}$$

$$= \frac{A \in_0}{2d} (1 + \in_r)$$

 $C_{\text{net}} = \frac{C_o}{2} (1 + \epsilon_r)$ 

Q.18 A rectifier is shown below. The diode and thyristor are ideal switches. The load contains  $R = 10 \Omega$  and L = 0.05 H. The firing angle  $\alpha$  in degrees to obtain a load voltage of 70 V



Solution: (29.42°)

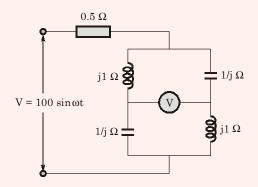
 $\Rightarrow$ 

$$V_o = \frac{V_m}{2\pi} (1 + \cos \alpha)$$
$$70 = \frac{235}{2\pi} (1 + \cos \alpha)$$

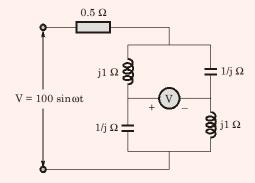
$$\frac{70 \times 2\pi}{235} \; = (1 + \cos\alpha)$$

 $\alpha = 29.42^{\circ}$ 

Q.19 What is the value of V in given figure.



Solution: (236 V)



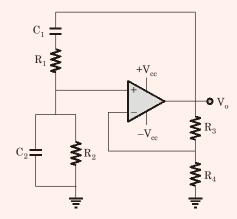
It is a balanced Wheatstone bridge with

$$Z_1 Z_4 = Z_2 Z_3$$

$$\Rightarrow \qquad \qquad \mathbf{j} \times \mathbf{j} = \frac{1}{\mathbf{i}} \times \frac{1}{\mathbf{i}}$$

Reading of voltmeter = 0 V*:*.

Q.20 Find the condition to balance the Wein's bridge.



$${\rm (a)} \quad \frac{R_3}{R_4} = \frac{R_1}{R_2}, \, \omega = \frac{1}{\sqrt{R_1 R_2 C_1 C_2}} \label{eq:alpha}$$

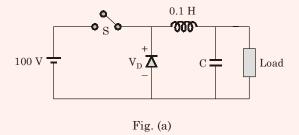
(b) 
$$\frac{R_2}{R_1} = \frac{C_2}{C_1}$$
,  $\omega = \frac{1}{R_1C_1R_2C_2}$ 

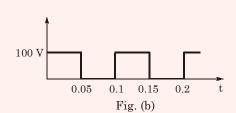
$$\text{(c)} \quad \frac{R_3}{R_4} = \frac{R_1}{R_2} + \frac{C_2}{C_1}, \, \omega = \frac{1}{\sqrt{R_1C_1R_2C_2}} \qquad \qquad \text{(d)} \quad \frac{R_2}{R_4} + \frac{R_1}{R_2} = \frac{C_2}{C_1}, \, \omega = \frac{1}{R_1C_1R_2C_2}$$

(d) 
$$\frac{R_2}{R_4} + \frac{R_1}{R_2} = \frac{C_2}{C_1}$$
,  $\omega = \frac{1}{R_1C_1R_2C_2}$ 

Solution: (c)

Q.21 Given figure shows a circuit diagram of a chopper. The switch 'S' in the circuit in Fig. (a) is switched ON such that the voltage across diode has the wave shape shown in Fig. (b). The capacitor C is large, so that the voltage across it is constant. If switch S and the diode are ideal, the peak to peak ripple (in A) in the inductor current is \_\_\_\_\_.





### Solution:(25 A)

The given circuit is a buck regulator,

$$V_o = V_s \times \frac{t_1}{T}$$

$$V_0 = 100 \times \frac{0.05}{0.1}$$

 $V_0 = 50 \, V$ *:*.

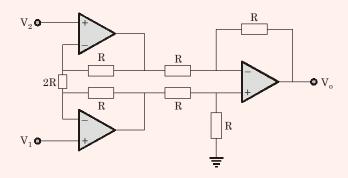
The peak-to-peak inductor ripple current,

$$\Delta I = \frac{V_o \times t_2}{L}$$

$$=\frac{50\times0.05}{0.1}$$

$$\Delta I = 25 A$$

### **Q.22** Find value of $V_0$ .



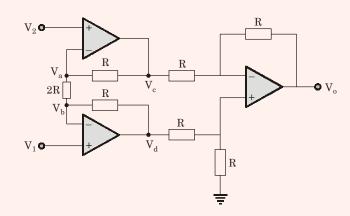
(a) 
$$\frac{1}{2}(V_1 - V_2)$$

(b) 
$$V_1 + V_2$$

(c) 
$$2(V_1 - V_2)$$

(d) 
$$V_1 - V_2$$

### Solution: (c)



$$V_o = -V_c \times \left(\frac{R}{R}\right) + V_d \times \frac{R}{2R} \left(1 + \frac{R}{R}\right)$$
$$= -V_c + \frac{V_d}{2} \times 2 = V_d - V_c$$

$$\begin{array}{lll} \text{and,} & -\mathrm{V_c} + \mathrm{IR} + \mathrm{I}(2\mathrm{R}) + \mathrm{IR} + \mathrm{V_d} = 0 \\ \\ \Rightarrow & \mathrm{V_d} - \mathrm{V_c} = -4 \, \mathrm{IR} \\ \\ \text{and,} & -\mathrm{V_a} + 2 \, \mathrm{IR} + \mathrm{V_b} = 0 \\ \\ \Rightarrow & 2 \, \mathrm{IR} = \mathrm{V_a} - \mathrm{V_b} \\ \\ \therefore & \mathrm{V_o} = -4 \, \mathrm{IR} \\ \\ & = -2(\mathrm{V_a} - \mathrm{V_b}) \\ \\ & = 2(\mathrm{V_b} - \mathrm{V_a}) \\ \\ \text{Here,} & \mathrm{V_1} = \mathrm{V_b} \\ \\ & \mathrm{V_2} = \mathrm{V_a} \\ \\ \therefore & \mathrm{V_o} = 2(\mathrm{V_1} - \mathrm{V_2}) \end{array}$$

Q.23  $A = \begin{bmatrix} 0 & 1 & -1 \\ -6 & -11 & 6 \\ -6 & -11 & 5 \end{bmatrix}$ , absolute value of the ratio of maximum eigen value to minimum

eigen value is

Solution: (1/3)

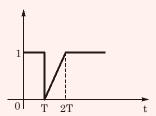
$$0 = |A - \lambda I|$$

$$0 = \begin{vmatrix} 0 & 1 & -1 \\ -6 & -11 & 6 \\ -6 & -11 & 5 \end{vmatrix} - \begin{bmatrix} \lambda & 0 & 0 \\ 0 & \lambda & 0 \\ 0 & 0 & \lambda \end{vmatrix}$$

$$0 = \begin{bmatrix} -\lambda & 1 & -1 \\ -6 & -11 - \lambda & 6 \\ -6 & -11 & 5 - \lambda \end{bmatrix}$$

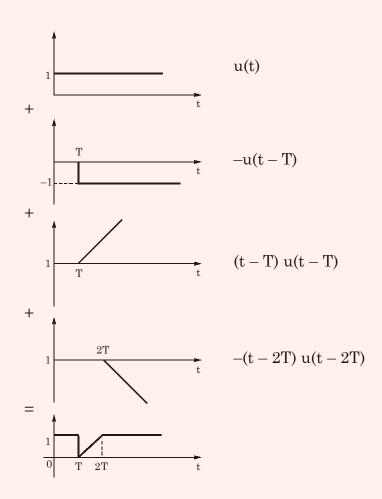
$$\begin{split} \left[ -\lambda (-55 - 5\lambda + 11\lambda + \lambda^2 + 66) + 1(-36 + 30 - 6\lambda) - 1(66 - 66 - 6\lambda) \right] &= 0 \\ (-\lambda^3 - 6\lambda^2 - 11\lambda) - 6 - 6\lambda + 6\lambda &= 0 \\ \lambda^3 + 6\lambda^2 + 11\lambda + 6 &= 0 \\ \lambda &= -1, -2, -3 \\ \left| \frac{\lambda_{max}}{\lambda_{min}} \right| &= \frac{1}{3} \end{split}$$

Q.24 Select the suitable representation of the below signal.



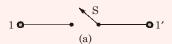
[Note: Options are not available]

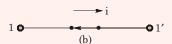
Solution: f(t) = u(t) - u(t - T) + (t - T) u(t - T) - (t - 2T) u(t - 2T)

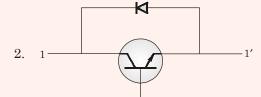


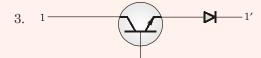
$$\therefore \qquad \qquad f(t) = u(t) - u(t-T) + (t-T) \ u(t-T) - (t-2T) \ u(t-2T)$$

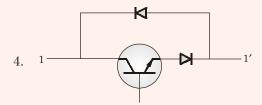
Q.25 An electronics switch S is required to block voltage of either polrity during its OFF state as shown in the figure (a). This swich is required to conduct in only one direction in its ON state as shown in the figure (b).











Which of the following are valid realizations of the switch S?

(a) Only 1

(b) 1 and 2

(c) 1 and 3

(d) 3 and 4

Solution: (c)

Q.26 In formation of Routh Hurwitz array all the row elements are zero. The premature termination shows

(a) One root at origin

- (b) Only one positive real root
- (c) Only one negative real root
- (d) Imaginary roots

Solution: (d)

Q.27 A 8 pole, 3 phase, 50 Hz induction machine is operating at 700 rpm, frequency of rotor current is \_\_\_\_\_ Hz.

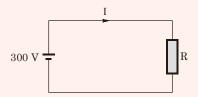
Solution: (3.33)

As 
$$n_{\rm s} = \frac{120 {\rm f}}{{\rm P}}$$
 
$$= \frac{120 \times 50}{8} = 750 \ {\rm rpm}$$
 
$${\rm s} = \frac{n_{\rm s} - n_{\rm r}}{n_{\rm s}} = \frac{750 - 700}{750} = \frac{50}{750} = \frac{1}{15}$$

Frequency of rotor current = sf

$$=\frac{1}{15} \times 50 = 3.33 \text{ Hz}$$

**Q.28** For circuit shown below, R = 25 + I/2. Find the value of I.



Solution: (10 A)

$$V = IR$$

$$\Rightarrow 300 = I\left(25 + \frac{I}{2}\right)$$

$$\Rightarrow 300 = 25I + \frac{I^2}{2}$$

$$\Rightarrow I^2 + 50I - 600 = 0$$

$$\Rightarrow I = 10 \text{ A or } -60 \text{ A}$$

$$\Rightarrow R = \left(25 + \frac{10}{2}\right) = 30$$
or
$$R = \left(25 - \frac{60}{2}\right) = -5$$

As resistance cannot be negative.

$$\therefore$$
 Value of I = 10 A



 $\textbf{Q.29} \hspace{0.2cm} x(t) \hspace{0.1cm} \text{is non-zero only for} \hspace{0.1cm} T_x < t < T_x' \hspace{0.1cm} \text{and similarly, } y(t) \hspace{0.1cm} \text{is non zero only for} \hspace{0.1cm} T_y < t < T_y'.$ 

Let z(t) be convolution of x(t) and y(t). Which one of the following statement is true?

- (a) z(t) can be non zero over an unbounded interval
- (b) z(t) is non zero for  $t < T_x + T_y$
- (c) z(t) is zero outside of  $T_x + T_y < t < T_x' + T_y'$
- (d) z(t) in non zero for  $t > T'_x + T'_y$

### Solution: (c)

Q.30 The vector field are given in Cartesian co-ordinate system. The vector field which does not satisfy the property of magnetic flux density is

(a) 
$$y^2 \hat{a}_x + z^2 \hat{a}_v + x^2 \hat{a}_z$$

(b) 
$$z^2 \hat{a}_x + x^2 \hat{a}_y + y^2 \hat{a}_z$$

(c) 
$$x^2 \hat{a}_x + y^2 \hat{a}_y + z^2 \hat{a}_z$$

(d) 
$$y^2z^2a_x + x^2z^2a_y + x^2y^2a_z$$

### Solution: (c)

According to Maxwell fourth equation,

$$\nabla \cdot \mathbf{B} = 0$$

Among the given options, only option (c) is not satisfying above criteria.

**Q.31** The solution for differential equation,  $\frac{d^2x}{dt^2} = -9x$  with initial condition,  $x(0^-) = 1$  and

$$\frac{\mathrm{dx}}{\mathrm{dt}}\Big|_{t=0} = 1 \text{ is}$$

(a) 
$$t^2 + t + 1$$

(b) 
$$\sin 3t + \frac{1}{2}\cos 3t + \frac{2}{3}$$

(c) 
$$\frac{1}{3}\sin 3t + \cos 3t$$

(d) 
$$\cos 3t + t$$

### Solution: (c)

$$\frac{d^2x}{dt^2} = -9x$$

Using Laplace transform,

$$s^{2} X(s) - sx(0^{-}) - x'(0^{-}) = -9X(s)$$
$$s^{2} X(s) - s(1) - (1) = -9 X(s)$$
$$X(s) (s^{2} + 9) = s + 1$$



$$X(s) = \frac{s+1}{s^2+9}$$

$$= \frac{s}{s^2+9} + \frac{1}{s^2+9} = \frac{s}{s^2+9} + \frac{1}{3} \left(\frac{3}{s^2+9}\right)$$

$$= \cos 3t + \frac{1}{3} \sin 3t$$

### **Alternative Solution:**

$$\frac{d^2x}{dt^2} + 9x = 0$$

$$D^2 + 9 = 0$$

$$D = \pm 3i$$

$$x = A\cos 3t + iB\sin 3t$$

$$x(0) = 1 = A$$
and
$$\frac{dx}{dt}\Big|_{t=0} = 1 = i3B$$

$$\therefore \qquad \qquad B = \frac{1}{3i}$$

$$\Rightarrow \qquad \qquad x = \cos 3t + \frac{1}{3}\sin 3t$$

**Q.32** If  $f(x) = xe^{-x}$ , the maximum value of the function in the interval  $(0, \infty)$  is,

(a) 
$$e^{-1}$$

(c) 
$$1 - e^{-1}$$

(d) 
$$1 + e^{-1}$$

### Solution: (a)

$$f(x) = xe^{-x}$$

$$f'(x) = e^{-x} + x(-e^{-x})$$

$$= e^{-x} - xe^{-x}$$

$$\Rightarrow \qquad f'(x) = 0$$

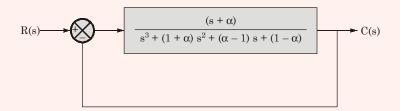
$$\Rightarrow \qquad e^{-x}(1-x) = 0$$

$$\Rightarrow \qquad x = 1, \infty$$

$$f''(x) = -e^{-x} + xe^{-x} - e^{-x}$$
at  $x = 1$ ,
$$= -2e^{-1} + (1)e^{-(1)}$$

$$= -e^{-1} < 0$$
at  $x = 1$ ,
$$f(1) = (1)e^{-1} = e^{-1}$$

**Q.33** For what minimum value of  $\alpha$ , the system will be stable



Solution:  $(\alpha = 0.618)$ 

Characteristic equation,

$$1 + G(s) H(s) = 0$$

$$s^{3} + (1 + \alpha)s^{2} + (\alpha - 1) s + (1 - \alpha) + (s + \alpha) = 0$$

$$\Rightarrow s^{3} + (1 + \alpha)s^{2} + s(\alpha - 1 + 1) + (1 - \alpha + \alpha) = 0$$

$$\Rightarrow s^{3} + (1 + \alpha)s^{2} + \alpha s + 1 = 0$$

By Routh array analysis,

For stable system,

$$1+\alpha>0$$
 i.e. 
$$\alpha>-1 \qquad \qquad ...(i)$$

$$\frac{\alpha(1+\alpha)-1}{1+\alpha} > 0$$

$$\alpha(1+\alpha)-1>0$$

$$\alpha = \frac{-1 - \sqrt{5}}{2}, \ \frac{-1 + \sqrt{5}}{2}$$

$$\alpha > 0.618$$
 and  $\alpha < -1.62$  ...(ii)

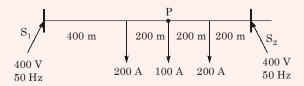
From equations (i) and (ii)

Minimum value of  $\alpha = 0.618$ .

- Q.34 The undesirable property of electrical insulating material is
  - (a) high dielectric strength
- (b) high relative permittivity
- (c) high thermal conductivity
- (d) high insulation resistivity

### Solution: (c)

**Q.35** The transmission line is fed from both end with source  $S_1$  and  $S_2$  of 400 V, 50 Hz each. The transmission line is 1 km long and has some resistance  $(m/\Omega)$  and negligible reactance.



What is the contribution of each source  $S_1$  and  $S_2$  from the both end to supply 100 A at point Prespectively?

(a) 20 A, 80 A

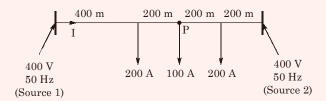
(b) 100 A, 0 A

(c) 0 A, 100 A

(d) 80 A, 20 A

### Solution: (c)

*:*.



Let current I is supplied by source 1, r be the resistance per unit length

∴ By KVL law

$$\Rightarrow$$
 -400 + (r × 400)I + (200r) (I - 200) + 200r (I - 300) + 200r (I - 500) + 400 = 0

$$\Rightarrow$$
 400 Ir + 200 Ir - 40000r + 200 Ir - 60000r + 200 Ir - 100000r = 0

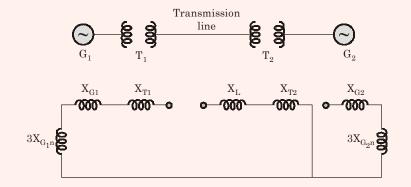
I = 200 A

$$\Rightarrow$$
 1000 Ir = 200000r

$$\therefore$$
 Contribution of source 1 to 100 A load at point P = 0 A.

and contribution of source 2 to 100 A load at point P = 100 A.

Q.36 The below diagram shown the zero sequence impedance diagram. Find the connection of both transformers  $T_1$  and  $T_2$ .



(a) 
$$\downarrow$$
- $\downarrow$  and  $\downarrow$ - $\downarrow$ 

(b) 
$$\Delta$$
 and  $\Delta$ -

(c) 
$$\Delta$$
 and  $\Delta$ 

(d) 
$$\downarrow -\Delta$$
 and  $\Delta -\Delta$ 

Solution: (c)

Q.37 In a 1-\$\phi\$ ac voltage regulator, the rms source voltage is 220 V ac, 50 Hz. Inductance of the coil is 16 mH and resistance is given as 5  $\Omega$ . Find the rms thyristor current and angle  $\phi$ ?

**Solution:** 

The rms thyristor current =  $I_{Tr} = \frac{V_s}{\sqrt{R^2 + (\omega L)^2}}$ 

$$= \frac{220}{\sqrt{5^2 + (2 \times \pi \times 50 \times 16 \times 10^{-3})^2}}$$

$$I_{Tr} = 32 A$$

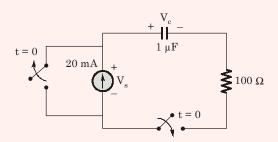
The load angle

$$\phi = \tan^{-1} \left( \frac{\omega L}{R} \right)$$

$$= \tan^{-1} \left( \frac{2\pi \times 50 \times 16 \times 10^{-3}}{5} \right)$$

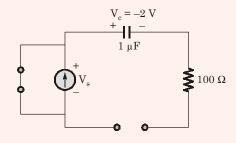
$$\phi = 45^{\circ}$$

**Q.38** Consider the circuit shown below. Given  $V_c(0) = -2$  V. The value of voltage  $(V_s)$  across the current source in the circuit is



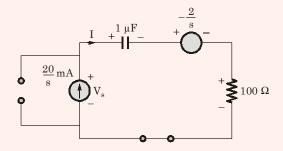
### Solution:

At 
$$t = 0^{-}$$



$$\therefore \qquad \qquad V_{s} = \left. 0 \; V \, \right|_{t \, = \, 0^{-}}$$

At 
$$t = 0^{+}$$



By KVL,

$$\left(\frac{-2}{s}\right) + \frac{I}{sC} + 100I = V_s$$

$$-2 \quad 20 \times 10^{-3} \qquad 1 \qquad 20 \times 10^{-3}$$

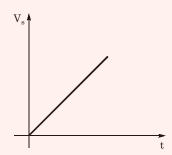
$$\Rightarrow \quad \frac{-2}{s} + \frac{20 \times 10^{-3}}{s} \times \frac{1}{s \times 10^{-6}} + 100 \times \frac{20 \times 10^{-3}}{s} \ = V_s$$

$$\Rightarrow \qquad \qquad V_s = -\frac{2}{s} + \frac{20 \times 10^3}{s^2} + \frac{2}{s}$$

$$V_{s}(s) = \frac{2}{s^2} \times 10^4$$

$$\therefore \qquad V_{s}(t) = 2 \times 10^{4}t$$

*:*.



- Q.39 For a specified input voltage and frequency, if the equivalent radius of the core of a transformer is reduced by half, the factor by which the number of turns in the primary should change to maintain the same no load current.

(c) 2

Solution: (d)

As

$$E = \sqrt{2}\pi f \phi N$$

where,

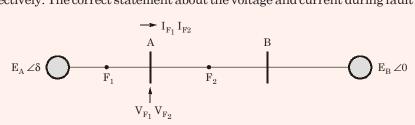
$$\phi = B \times A$$

- : Radius is reduced by half
- $\therefore$  Area get reduced to  $\frac{1}{4}$ .

To maintain no load current constant,

we have to maintain E constant.

- ⇒ Number of turns in the primary should be increased by 4 times.
- **Q.40** If the fault takes place of  $F_1$  then the voltage and the current at bus A are  $V_{F1}$  and  $I_{F1}$ respectively. If the fault occurs at  $\boldsymbol{F}_{2}\!,$  the Bus A voltage and current are  $\,\boldsymbol{V}_{F_{2}}$  and  $\boldsymbol{I}_{F_{2}}$ respectively. The correct statement about the voltage and current during fault  $F_1$  and  $F_2$  is



- (a)  $V_{F_1}$  leads  $I_{F_1}$  and  $V_{F_2}$  leads  $I_{F_2}$  (b)  $V_{F_2}$  leads  $I_{F_1}$  and  $V_{F_2}$  lags  $I_{F_2}$
- (c)  $V_{F_2}$  lags  $I_{F_1}$  and  $V_{F_2}$  leads  $I_{F_2}$  (d)  $V_{F_2}$  lags  $I_{F_1}$  and  $V_{F_2}$  lags  $I_{F_2}$

### Solution: (a)

In case of fault at  $F_1$ ,

 $V_{F_i}$  lead  $I_{F_i}$ 

Similarly, in case of fault at  $F_2$  also,  $V_{F_2}$  leads  $I_{F_2}$  as fault always demands reactive power.

- **Q.41** In an unbalanced 3- $\phi$  system, phase current  $I_a = 1 \angle -90^{\circ}$  p.u., negative sequence current  $I_{b_2}$  = 4/-150° p.u., zero sequence current,  $I_{C_0}$  = 3/90° p.u. Then, magnitude of phase current  $I_b$  in p.u. is
  - (a) 1.00

(b) 7.81

(c) 11.53

(d) 13.00

### Solution: (c)

$$I_a = 1 \angle -90^{\circ} \text{ p.u.}$$

$$I_{b_2} = 4 \angle -150^{\circ} \text{ p.u.}$$

$$I_{c_0} = 3 \angle 90^{\circ} \text{ p.u.}$$

$$I_{a} = I_{a_{1}} + I_{a_{2}} + I_{a_{0}}$$

$$I_{b_9} = \alpha I_{a_9}$$

∴ 
$$4\angle -150^{\circ} = 1\angle 120^{\circ} I_{a_2}$$

$$I_{a_2} = \frac{4\angle -150^{\circ}}{1\angle 120^{\circ}}$$

$$= 4\angle -270^{\circ}$$

$$I_{a_0} \ = \ I_{b_0} = I_{c_0} = 3 \angle 90^\circ$$

$$I_{a_1} = 1\angle -90^{\circ} - 4\angle -270^{\circ} - 3\angle 90^{\circ}$$
$$= +8\angle -90^{\circ}$$

$$\Rightarrow$$
  $I_{b_1} = \alpha^2 I_{a_1}$ 

$$= 1 \angle 240^{\circ} \times 8 \angle -90^{\circ} = 8 \angle 150^{\circ}$$

$$\begin{aligned} & = I_{b_1} + I_{b_2} + I_{b_0} \\ & = 8 \angle 150^\circ + 4 \angle -150^\circ + 3 \angle 90^\circ \\ & = 11.53 \angle 154.3^\circ \text{ p.u.} \end{aligned}$$

- Q.42 The core loss of a 1-\$\phi\$ 230/115 V, 50 Hz power transformer is measured from 230 V side by feeding the primary 230 V side from a variable voltage variable frequency source with keeping the secondary open circuit, the core loss is measured to be 1050 W for 230 V, 50 Hz input. The core loss again measured to be 500 W for 138 V, 30 Hz input. The hysteresis and eddy current loss of transformer for 230 V, 50 Hz input are respectively.
  - (a) 508 W and 542 W

(b) 468 W and 582 W

(c) 498 W and 552 W

(d) 488 W and 562 W

### Solution: (a)

When

$$V = 230 V$$

$$f = 50 Hz$$

Core losses = 1050 W

Iron loss + Hysteresis loss = 1050 W

Iron loss = 
$$P_i = K_i V^2$$

 ${\rm Hysteresis\,loss} = {\rm P_H} = {\rm K_H}\,{\rm V}^{1.6}\,{\rm f}^{-0.6}$ 

$$\Rightarrow K_{i}(230)^{2} + K_{H} \frac{(230)^{1.6}}{(50)^{0.6}} = 1050 \qquad ...(i)$$

When

$$V = 138 V$$

$$f = 30 Hz$$

core losses = 500 W

$$\Rightarrow$$

$$P_{i} + P_{H} = 500$$

$$\Rightarrow K_{i}(138)^{2} + K_{H} \frac{(138)^{1.6}}{(30)^{0.6}} = 500 \qquad ...(ii)$$

Equation (i)

$$\Rightarrow$$
 52900 K<sub>i</sub> + K<sub>H</sub> 574.62 = 1050 ...(iii)

Equation (ii)

$$\Rightarrow$$
 19044 K<sub>i</sub> + K<sub>H</sub> 344.77 = 500 ...(iv)

Solving equations (iii) and (iv)

$$K_i = 0.01024$$

$$K_{H} = 0.885$$

:. Hysteresis loss at 230 V and 50 Hz

$$= 0.885 \times 574.62$$

and

Eddy loss = 
$$0.01024 \times 52900$$

= 541.69 W

Q.43 An incandescent lamp is marked 40 W, 240 V. If resistance at room temperature (26°C) is  $120 \Omega$  and temperature coefficient is  $4.5 \times 10^{-3}$  C then "ON" state filament temperature in °C is approximately \_\_\_\_\_

### Solution: (2470.44°C)

$$P = 40 \text{ W}$$

$$V = 240 \text{ V}$$

$$\therefore \qquad R_{\theta} = \frac{V^2}{P} = \frac{(240)^2}{40} = 1440 \Omega$$
At
$$t = 26^{\circ}$$

$$R = 120 \Omega$$

$$\alpha = 4.5 \times 10^{-3}/^{\circ}\text{C}$$

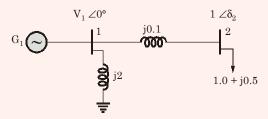
$$R_{\theta} = R[1 + \alpha (\theta_2 - \theta_1)]$$

$$\Rightarrow \qquad 1440 = 120 \left[1 + 4.5 \times 10^{-3} (\theta_2 - 26)\right]$$

$$2444.44 = \theta_2 - 26^{\circ}$$

$$\theta_2 = 2470.44^{\circ}\text{C}$$

**Q.44** Find the value of  $V_1$  in p.u. and  $\delta_2$  respectively.



(a) 0.95 and ∠6.00°

(b)  $1.05 \text{ and } \angle -5.44^{\circ}$ 

(c) 1.1 and ∠6.00°

(d)  $1.1 \text{ and } \angle -27.12^{\circ}$ 

### Solution:

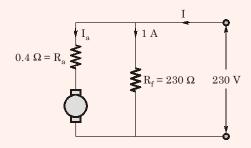
$$\begin{split} \frac{V_1 \angle 0^\circ - 1 \angle \delta_2}{0.1 \angle 90^\circ} &= I \angle \theta = 1 + j0.5 \\ \\ \Rightarrow & V_1 \angle 0^\circ - 1 \angle \delta_2 = 0.11 \angle 116.56^\circ \\ \\ V_1 - (\cos \delta_2 + j \sin \delta_2) &= 0.11 \left[ \cos 116.56^\circ + j \sin 116.56^\circ \right] \end{split}$$

On comparing, real and imaginary terms

We get,  $V_1 = 0.95$  $\delta_{2} = \angle 6.00^{\circ}$ and

Q.45 A 15 kW, 230 V dc shunt motor has armature circuit resistance 0.4  $\Omega$  and field circuit resistance of 230  $\Omega$ . At no load and rated voltage, the motor runs at 1400 rpm and the line current drawn by the motor is 5 A. At full load, the motor draws a line current of 70 A. Neglect armature reaction. The full load speed of the motor in rpm is \_\_\_\_\_.

### Solution: (1241.1 rpm)



At no load,

$$n = 1400 \text{ rpm}$$

$$I = 5A$$

$$\begin{split} \mathbf{I} &= \mathbf{I_f} + \mathbf{I_a} \\ \mathbf{I_a} &= 5 - 1 = 4 \; \mathbf{A} \end{split}$$

$$230 = E_{f_1} + 4 \times 0.4$$

$$230 - 1.6 = E_{f_1}$$

$$\Rightarrow$$
 228.4 V =  $E_{f_1}$ 

At full load,

As

$$I = 70 A$$

$$\Rightarrow$$
  $I_a = I - I_f$ 

$$= 70 - 1 = 69$$
A

$$E_{f_2} = 230 - 69 \times 0.4$$

$$= 230 - 27.6$$

$$= 202.4$$

 $E_{\rm c} \propto \phi \omega$ 

For DC shunt motor, \$\phi\$ is constant

$$\therefore \hspace{1cm} E_{\rm f} \sim \omega$$

$$\Rightarrow \qquad \qquad \frac{E_{f_1}}{E_{f_2}} \; = \; \frac{\omega_1}{\omega_2}$$

$$\Rightarrow \frac{228.4}{202.4} = \frac{1400}{N_2}$$

$$\Rightarrow$$
  $N_2 = \frac{1400}{1.128} = 1241.1 \text{ rpm}$ 

**Q.46** A 3- $\phi$  50 Hz, 6 pole induction motor has rotor resistance 0.1  $\Omega$  and reactance 0.92  $\Omega$ . Neglect the voltage drop in stator and assume that the rotor resistance is constant. Given the full load slip 3%. The ratio of maximum torque to full load torque is \_\_\_\_.

### **Solution: (1.948)**

$$r_2 = 0.1 \Omega$$
 and  $x_2 = 0.92 \Omega$ 

$$T_{\rm fl} = \frac{2T_{\rm em}}{\frac{s_{\rm mT}}{s_{\rm fl}} + \frac{s_{\rm fl}}{s_{\rm mT}}}$$

where, 
$$T_{\rm fl} = {\rm Full \, load \, torque}$$
 
$$T_{\rm em} = {\rm Maximum \, torque}$$

$$s_{mT} = Slip at maximum torque$$

$$s_{fl} = Slip at full load$$

As 
$$s_{fl} = 3\% = 0.03$$

and 
$$s_{mT} = \frac{r_2}{x_2} = \frac{0.1}{0.92}$$

$$\frac{T_{em}}{T_{fl}} = \frac{\frac{s_{mT}}{s_{fl}} + \frac{s_{fl}}{s_{mT}}}{2}$$

$$= \frac{\left(\frac{10}{92}}{0.03}\right) + \left(\frac{0.03}{\frac{10}{92}}\right)}{2}$$

$$= \frac{3.62 + 0.276}{2} = 1.948$$

Q.47 The fuel constant of two power plants are

$$\label{eq:P1} {\rm P}_1 \ : \ {\rm C}_1 = \, 0.05 \; {\rm P}_{g_1}^2 \, + {\rm AP}_{g_1} \, + {\rm B}.$$

$$P_2 : C_2 = 0.10P_{g_2}^2 + 3AP_{g_2} + 2B.$$

When  $P_{g_1}$  and  $P_{g_2}$  are generated powers. If two plants optimally share 1000 MW load at incremental fuel constant of 100 Rs/MW, the ratio of load share by power plant 1 and power plant 2 is

(a) 1:4

(b) 2:3

(c) 3:2

(d) 4:1

### Solution: (d)

Given, 
$$C_1 = 0.05 P_{g_1}^2 + AP_{g_1} + B$$
 ...(i)

$$C_2 = 0.10P_{g_2}^2 + 3AP_{g_2} + 2B$$
 ...(ii)

and 
$$P_{g_1} + P_{g_2} = 1000$$
 ...(iii)

$$\frac{dC_1}{dP_{g_1}} = \frac{dC_2}{dP_{g_2}} = 100$$
 ...(iv)

$$\frac{dC_1}{dP_{g_1}} \ = \ 2 \times 0.05 \ P_{g1} + A = 100$$

and 
$$\frac{dC_2}{dP_{g_2}} \; = \; 2 \times 0.10 \; P_{g_2} + 3 \; A = 100$$

$$\therefore$$
 0.1  $P_{g_1} + A = 100$ 

$$0.2 P_{g_2} + 3 A = 100$$

$$\Rightarrow$$
 0.3  $P_{g_1} - 0.2 P_{g_2} = 200$  ...(v)

From equations (iv) and (v)

$$\therefore \qquad \qquad P_{g_1} \, = \, 800 \, \mathrm{MW}$$

and 
$$P_{g_2} = 200 \,\mathrm{MW}$$

$$\therefore \qquad \qquad \frac{P_{g_1}}{P_{g_2}} = \frac{4}{1}$$