



Detailed Solution (SET-C)

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SET - C

1. A reversed Carnot engine is used for heating a building. It supplies 210×10^3 kJ/hr of heat to the building at 20°C. The outside air is at -5°C. The heat taken from the outside will be nearly

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- (a) 192 × 10³ kJ/hr
- (b) 188 × 10³ kJ/hr
- (c) 184×10^3 kJ/hr
- (d) 180×10^3 kJ/hr
- Ans. (a)

Sol.

 $T_1 = 273 + 20 = 293 K$

$$T_2 = 273 - 5 = 268 \text{ K}$$

 $Q_1 = 210 \times 10^3 \text{ kJ/hr}$

For a reversed Carnot engine,



- 2. In an Electrolux refrigerator, a thermo-siphon bubble pump is used to lift the
 - (a) weak aqua solution from the generator to the separator
 - (b) weak aqua solution from the separator to the absorber
 - (c) strong agua solution from the generator to the separator
 - (d) strong agua solution from the generator to the evaporator

Ans. (a)

- Sol. In electrolux refrigerator, a thermosyphon bubble pump is used to lift the weak aqua solution from the generator to the seperator. The discharge tube from the generator is extended down below the liquid level in the generator. The bubbles rise and carry slugs of weak $NH_3 - H_2O$ solution into the seperator.
- 3. The enthalpy of moist air with normal notationas is given by

(a)
$$h = (1.005 + 1.88W) t + 2500W$$

(b)
$$h = 1.88Wt + 2500W$$

- (c) h = 1.005Wt
- (d) h = (1.88 + 1.005W) t + 2500W

Ans. (a)

Sol. Enthalpy of moist air, $h = h_a + w h_v$

⇒ h = 1.005 t + w [2500 + 1.88t] kJ/kgda

 \Rightarrow h = [1.005 + 1.88 w] t + 2500W

- If the relative humidity of atmospheric air is 4. 100%, then the wet-bulb temperature will be
 - (a) more than dry-bulb temperature
 - (b) equal to dew-point temperature
 - (c) equal to dry-bulb temperature
 - (d) less than dry-bulb temperature

Ans. (b, c)

- Sol. If relative humidity of atmospheric air is 100%, then air is saturated and for saturated air DBT = WBT = DPT
- 5. During an air-conditioning of a plant, the room sensible heat load is 40 kW and room latent heat load is 10 kW, ventilation air is 25% of supply air. At full load, the room sensible heat factor will be



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|--|---|--|--------------------|---|
| Ans. | (a) 0.9 (c) 0.7 (b) | (b) 0.8 (d) 0.6 | | supplied to the rotor(d) useful hydrodynamic energy in the fluid at final discharge and mechanical energy supplied to the shaft and coupling |
| Sol. 6. Ans. Sol. | 30cm, speed 350 r.p net brake load 610 N 1m, oil consumption of fuel 44×10^3 kJ/k efficiency will be (a) 29.1% (c) 33.5% (a) D = 20cr L = 30 c N = 350 | has bore of 20 cm, stroke b.m., i.m.e.p. 275 kN/m ² , l, diameter of brake drum 4.25 kg/hr, calorific value cg. The indicated thermal (b) 31.3% (d) 35.7% | Ans. Sol. 8. | (b) Hydraulic efficiency = Head extracted by the rotor Net load available to the rotor work done by the runner = K.E. of the jet inlet to bucket Mechanical energy supplied by the rotor = Hydrodynamic energy available from fluid Consider the following statements regarding compounding in steam turbines: 1. In impulse turbine, steam pressure |
| i.p. 7. | = 15118.9 × 10 ⁻³ W $\eta_{ip} = \frac{115}{4.2}$ = 0.29 The hydraulic efficient ratio of (a) mechanical energy available from the (b) mechanical energy and hydrodyname the fluid (c) useful hydrodyn | $\frac{10^{6} \text{ J/kg}}{25} \text{ kg/s}$ $\frac{25}{60} \text{ kg/s}$ $\frac{2}{30 \times 10^{-2} \times \frac{350}{60} \times 10^{3}}{5 \times 44 \times 10^{6}} \times 60 \times 60$ $1 = 29.1\%$ ency of a turbine is the rgy in the output shaft at hydrodynamic energy | Ans. Sol. | remains constant between ends of the moving blades. 2. In reaction turbine, steam pressure drops from inlet to outlet of the blade. 3. In velocity compounding, partial expansion of steam takes place in the nozzle and further expansion takes place in the rotor blades. Which of the above statements are correct? (a) 1 and 2 only (b) 1 and 3 only (c) 2 and 3 only (d) 1, 2 and 3 (a) In impulse turbine inlet pressure = outlet pressure and blade is equiangular So, change in relative component is zero and hence relative component is zero and hence relative component is same, so no reaction takes place. In reaction turbine steam pressure drops from inlet to outlet of the blade In velocity compounding whole expansion takes place in nozzle and velocity is |
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reduced subsequent stages.

- **9.** In a lawn sprinkler, water leaves the jet with an absolute velocity of 2m/s and the sprinkler arms are 0.1 m in length. The sprinkler rotates at a speed of 120 r.p.m. The utilization factor of this sprinkler will be nearly
 - (a) 0.72 (b) 0.64
 - (c) 0.56 (d) 0.49
- Ans. (a*)

Sol.

Consider sprinkles asradial blade

$$\eta = \frac{\left(\frac{2\pi N}{60} \times 0.1\right)^2}{\frac{(2)^2}{2}} = \frac{1.578}{2} = 0.788$$

- **10.** Which one of the following statements is correct with respect to axial flow 50% reaction turbine?
 - (a) The combined velocity diagram is symmetrical.
 - (b) The outlet absolute velocity should not be axial for maximum utilization
 - (c) Angles of both stator and rotor are not identical.
 - (d) For maximum utilization, the speed ratio



Ans. (a) Sol.



for maximum $'\eta'$

In 50% reaction turbine for maximum $^{\prime}\eta^{\prime}$

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$$\alpha_2 = 90^\circ$$
, $\alpha_3 = \alpha_2$, $\frac{U}{V_1} = \cos \alpha$

- **11.** In axial flow pumps and compressors, the combined velocity diagram with common base is used to determine change in
 - (a) absolute velocity $(V_2 V_1)$
 - (b) relative velocity $(V_{r_2} V_{r_1})$
 - (c) tangential velocity $(U_2 U_1)$
 - (d) whirl velocity $(V_{u_2} V_{u_1})$

Ans. (d)

Sol.



12. In a steam turbine with steam flow rate of 1 kg/s, inlet velocity of steam of 100 m/s, exit velocity of steam of 150 m/s, enthalpy at inlet of 2900 kJ/kg, enthalpy at outlet of 1600 kJ/kg, the power available from the turbine will be nearly

| (a) | 1575.5 kW | (b) | 1481.6 kW | |
|-----|-----------|-----|-----------|--|
| | | | | |

(c) 1387.7 kW (d) 1293.8 kW

Ans. (d)

(

Sol.

$$\Delta h_0$$
 = stagnation enthalpy

$$= \left(h_1 + \frac{v_1^2}{2}\right) - \left(h_2 + \frac{v_2^2}{2}\right)$$
$$= \left(2900 + \frac{1}{2}(100)^2 - 1600 - \frac{1}{2}(150)^2\right)$$



= 1293.8 kW

- **13.** In an isentropic flow through a nozzle, air flows at the rate of 600 kg/hr. At inlet to nozzle, the pressure is 2 MPa and the temperature is 127°C. The exit pressure is of 0.5 MPa. If the initial velocity of air is 300 m/s, the exit velocity will be
 - (a) 867 m/s (b) 776 m/s
 - (c) 685 m/s (d) 594 m/s

Ans. (d)

=

Sol.

$$\Gamma_1 = 127^{\circ}C = 273 + 127 = 400 \text{ K}$$

$$P_1 = 2MPa, P_2 = 0.5 MPa, V_1 = 300 m/se$$

$$\frac{T_1}{T_2} = \left(\frac{P_1}{P_2}\right)^{\frac{\gamma-1}{\gamma}} = \left(\frac{2}{0.5}\right)^{\frac{1.4-1}{1.4}}$$
$$= (4)^{0.285} = 1.484$$
$$T_2 = \frac{T_1}{1.484} = 269.54K$$
$$h_1 + \frac{V_1^2}{2} = h_2 + \frac{V_2^2}{2}$$
$$V_2 = \sqrt{2(h_1 - h_2) + (300)^2}$$
$$\sqrt{2 \times 1.005 \times 1000(400 - 269.5) + (300)^2}$$

= 594 m/sec

- 14. In a steam turbine, the nozzle angle at the inlet is 18°. The relative velocity is reduced to the extent of 6% when steam flows over the moving blades. The output of the turbine is 120 kJ/kg flow of steam. If the blades are equiangular, the speed ratio and the absolute velocity of steam ratio and the absolute velocity of steam at inlet for maximum utilization are nearly
 - (a) 0.42 and 230.2 m/s
 - (b) 0.48 and 230.2 m/s
 - (c) 0.42 and 515.1 m/s
 - (d) 0.48 and 515.1 m/s

Ans. (d)

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Sol.

$$\frac{V_b}{V_1} = \frac{\cos\alpha}{2} = 0.4755 \approx 0.48$$
$$(V_1 \cos\alpha_1 - V_b)(1 + K) \times V_b = 120 \times 10^3$$
$$(V_1 \cos 18 - 0.48V_1) \left(1 + \frac{94}{100}\right) \times 0.48V_1 = 120 \times 10^3$$
$$V_1^2 (\cos 18 - 0.48)(1.94) \times 0.48 = 120 \times 10^3$$

15. An air compressor compresses atmospheric air at 0.1 MPa and 27°C by 10 times of air inlet pressure. During compression, the heat lost to the surrounding is estimated to be 5% of compression work. Air enters the compressor with a velocity of 40 m/s and leaves with 100 m/s. The inlet and exit cross-sectional areas are 100 cm² and 20cm² respectively. The temperature of air at the exit from the compressor will be

 $V_1 \simeq 515.1 \text{ m/s}$

| (a) 1498 K | (b) 1574 K |
|------------|------------|
|------------|------------|

р

Ans. (a)

 \Rightarrow

$$\rho_1 = \frac{r_1}{RT_1} = \frac{0.1 \times 10}{0.287 \times 10^3 \times 300}$$
$$= 1.1614 \text{ kg/m}^3$$

 0.1×10^{6}

$$\dot{m} = \rho_1 A_1 V_1 = 1.1614 \times 100 \times 10^{-4} \times 40$$

= 0.4646 kg/s

$$\dot{m} = \rho_2 A_2 V_2 = \frac{P_2}{RT_2} A_2 V_2$$

 $P_2 A_2 V_2$

 $T_2 = -$

$$= \frac{1 \times 10^{6} \times 20 \times 10^{-4} \times 100}{0.4646 \times 0.287 \times 10^{3}}$$

= 1499.9 K

ṁR





16. A compressor delivers 4 m³ of air having a mass of 5 kg. The specific weight and specific volume of air being delivered will be nearly

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- (a) 12.3 N/m³ and 0.8 m³/kg
- (b) 14.6 N/m³ and 0.4 m³/kg
- (c) 12.3 N/m³ and 0.4 m³/kg
- (d) 14.6 N/m³ and 0.8 m³/kg

Ans. (a)

Sol.

Specific weight = $\frac{\text{weight}}{\text{volume}} = \frac{\text{mg}}{\text{V}}$

$$=\frac{5\times9.81}{4}=12.26$$
 N/m²

Specific volume = $\frac{\text{volume}}{\text{mass}}$

$$=\frac{4}{5}=0.8 \text{ m}^3/\text{kg}$$

- 17. In centrifugal compressors, there exists a loss of energy due to the mismatch of direction of relative velocity of fluid at inlet with inlet blade angle. This loss is known as
 - (a) frictional loss (b) incidence loss
 - (c) clearance loss (d) leakage loss
- Ans. (b)
- **Sol.** Additional losses that occur in a row of blades in a centrifugal compressor stage on account of incidence (mismatch of direction of relative velocity of fluid of inlet with inlet blade angle) termed as incidence losses. It is conventionally known as shock losses.
- 18. A centrifugal compressor develops a pressure ratio of 5 and air consumption of 30 kg/s. The inlet temperature and pressure are 15°C and 1 bar respectively. For an isentropic efficiency of 0.85, the power required by the compressor will be nearly

| (a) | 5964 kW | (b) 5778 kW |
|-----|---------|-------------|
| (c) | 5586 kW | (d) 5397 kW |

$$W = C_{p}T_{0} \left(r_{p}^{\frac{\gamma-1}{\gamma}} - 1\right)$$

= 1.005 × 288 ((5)^{0.4}/_{1.4} - 1)
= 1.005 × 288 × 0.5819
= 168.45 kW/kg
$$V_{ideal} = 167.615 \times 30 = 5053.62$$
$$\eta_{st} = \frac{W_{ideal}}{W_{actual}}$$
$$\eta_{st} = \frac{W_{ideal}}{\eta_{st}} = \frac{5053.62}{0.85}$$
$$= 5964 \text{ kW}$$

- **19.** The efficiency of superheat Rankine cycle is higher than that of simple Rankine cycle because
 - (a) the enthalpy of main steam is higher for superheat cycle
 - (b) the mean temperature of heat addition is higher for superheat cycle
 - (c) the temperature of steam in the condenser is high
 - (d) the quality of steam in the condenser is low

Ans. (b)

- **20.** In steam power cycle, the process of removing non-condensable gases is called
 - (a) scavenging process
 - (b) deaeration process
 - (c) exhaust process
 - (d) condensation process
- Ans. (b)
- **21.** The internal irreversibility of Rankine cycle is caused by
 - 1. fluid friction





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= [15×10⁵ × 0.3 – 1.5 × 10⁵ × 1.7634]/0.3 = 618.3 kJ

- **25.** Which of the following statements is/are correct regarding superheater in boilers?
 - 1. It is heat exchanger in which heat is transformed to the saturated steam to increase its temperature.
 - 2. It raises the overall efficiency.
 - 3. It reduces turbine internal efficiency.

Select the correct answer using the code given below.

| (a) | 1 | and | 2 | (b) | 1 | and | 3 |
|-----|---|-----|---|-----|---|-----|---|
| | | | | | | | |

(c) 2 and 3 (d) 1 only

Ans. (a)

- **Sol.** The superheater is a heat exchanger in which heat is transferred to the saturated steam to increase its temperature. It raises the overall efficiency. It reduces the moisture content in last stages of the turbine and thus increases the turbine internal efficiency.
- 26. Water vapour at 90 kPa and 150°C enters a subsonic diffuser with a velocity of 150 m/s and leaves the diffuser at 190 kPa with a velocity of 55 m/s, and during the process, 1.5 kJ/kg of heat is lost to the surrounding. For water vapour, C_p is 2.1 kJ/kgK. The final temperature of water vapour will be

| (a) | 154°C | | (b) | 158°C | |
|-----|-------|--|-----|-------|--|
| (c) | 162°C | | (d) | 166°C | |

Ans. (a)

Sol. Applying S.F.E.E. at inlet and exit of diffuser

$$h_{1} + \frac{V_{1}^{2}}{20w} + q_{cv} = h_{2} + \frac{V_{2}^{2}}{2000}$$
$$C_{p}(T_{2} - T_{1}) = \frac{V_{1}^{2} - V_{2}^{2}}{2000} - 1.5$$
$$\Rightarrow T_{2} = 154^{\circ}C$$

27. A steam turbine is supplied with steam at a pressure of 20 bar gauge. After expansion in

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the steam turbine, the steam passes to condenser which is maintained at a vacuum of 250 mm of mercury by means of pumps. The inlet and exhaust steam pressures will be nearly

- (a) 2101 kPa and 68 kPa
- (b) 2430 kPa and 78 kPa
- (c) 2101 kPa and 78 kPa
- (d) 2430 kPa and 68 kPa

Ans. (a)

Sol. Inlet pressure = 20 bar guage

Absolute inlet pressure = Guage Pr. + atmospheric

Exit pressure = 250 mm of mercury (vaccum)

Absolute exit pressure = Atmospheric pressure - vaccum pressure

= (101 - 13.6 × 9.81 × 0.25) kPa

= 67.64 kPa

28. In a power plant, the efficiencies of the electric generator, turbine, boiler, thermodynamic cycle and the overall plant are 0.97, 0.95, 0.92, 0.42 and 0.33 respectively. The total electricity generated for running the auxiliaries will be nearly

| (a) 4.9% | (b) 5.7% |
|----------|----------|
| (c) 6.5% | (d) 7.3% |

Ans. (d)

Sol. Overall efficiency = $\eta_q \times \eta_t \times \eta_b \times \eta_c \times \eta_a$

$$0.33 = 0.97 \times 0.95 \times 0.92 \times 0.42 \times \eta_a$$

 $\eta_a = 0.926$

The total electricity generated for running auxilliarities = 1 - 0.926 = 0.073 or 7.3%

- **29.** A turbine in which steam expands both in nozzle as well as in blades is called as
 - (a) impulse reaction turbine



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(b) 645 MPa

(d) 615 MPa



$$= 460 \left(\frac{12.8}{10.7} \right) 2$$

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= 658.3 MPa

34. An iron container $10 \text{cm} \times 10 \text{cm}$ at its base is filled to a height of 20 cm with a corrosive liquid. A current is produced as a result of an electrolytic cell, and after four weeks, the container has decreased in weight by 70 g. If n = 2, F = 96500 C and M = 55.84 g/mole, the current will be

| (a) | 0.05 A | (b) | 0.10 A |
|-----|--------|-----|--------|
| | | | |

(c) 0.20 A (d) 0.40 A

Ans. (b)

Sol. Total exposure time = $4 \times 7 \times 24 \times 3600 = 2.42 \times 10^6$ s

As per Faraday's law,

$$m = \frac{QM}{nF} = \frac{ItM}{nF}$$

where Q = charge, F = current,

F = Faraday's constant = 96500 C

n = no. of equivalents (mols of electrons) transferred per mol of metal

m = mass of metal oxidised (g)

M = molecular wt. of metal (g/mole)

$$\Rightarrow I = \frac{mnF}{tM} = \frac{70 \times 2 \times 96500}{(2.42 \times 10^6 \times 55.84)} = 0.1A$$

- **35.** A copper piece originally 305 mm long is pulled in tension with a stess of 276 MPa. If the deformation is entirely elastic and the modulus of elasticity is 110 GPa, the resultant elongation will be nearly
 - (a) 0.43 mm (b) 0.54 mm
 - (c) 0.65 mm (d) 0.77 mm
- Ans. (d)

Sol. Elongation,
$$\delta \ell = \frac{\sigma \ell}{E} = \frac{276 \times 305}{110 \times 10^3} = 0.77 \, \text{mm}$$

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36. The indentation on a steel sample has been taken using 10 mm tungsten carbide ball at 500 kgf load. If the average diameter of the indentation is 2.5 mm, the BHN will be nearly

Ans. (b)

Sol. Brinell hardness number,

BHN =
$$\frac{F}{\frac{\pi D}{2} (D - \sqrt{D^2 - d^2})}$$
$$= \frac{2 \times 500}{\pi \times 10 [10 - \sqrt{10^2 - 2.5^2}]}$$
$$= 100$$

- **37.** Which of the following statements are correct with respect to inversion of mechanisms?
 - 1. It is a method of obtaining different mechanisms by fixing different links of the same kinematic chain.
 - 2. It is method of obtaining different mechanisms by fixing the same links of different kinematic chains.
 - 3. In the process of inversion, the relative motions of the links of the mechanisms produced remain unchanged.
 - 4. In the process of inversion, the relative motions of the links of the mechanisms produced will change accordingly.

Select the correct answer using the code given below.

- (a) 1 and 3 (b) 1 and 4
- (c) 2 and 3 (d) 2 and 4

Ans. (a)

38. For the follower with stroke S, following the cycloidal motion, the radius of the rolling circle will be

(a)
$$S \times 2\pi$$
 (b) $\frac{S}{2\pi}$



ESE-2019 Conventional Test Schedule, Mechanical Engineering

| Date | Торіс | | | | |
|-----------------|---|--|--|--|--|
| 17th Mar 2019 | N.T. : TH-1, TH-2, HT-1, RAC-1, MS-1, MS-2 | | | | |
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| 07th Apr 2019 | N.T.: FMM-2, PPE-1,RSE-2 | | | | |
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| 14th Apr 2019 | N.T.: ICE-1,ToM-2, MR-1 | | | | |
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| 21st Apr 2019 | N.T. : ToM-1, MR-2, PROD-1 | | | | |
| | R.T. : MS-1, MECH-1, MECH-2,TH-1 | | | | |
| 28th Apr 2019 | N.T. : IE-1, PPE-2, FMM-3, | | | | |
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| 12th May 2019 | N.T.: ToM-3, ICE-2 | | | | |
| | R.T. : MR-2, RSE-1, RSE-2, HT-1, HT-2, FMM-2 | | | | |
| 19th May 2019 | N.T.: RE-2, MD-1 | | | | |
| | R.T. : PPE-1, PPE-2, FMM-3, ToM-2, ToM-3 | | | | |
| 26th May 2019 | N.T. : Mech-3, MD-2 | | | | |
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| 09th Jun 2019 | Full Length-2 (Test Paper-1 + Test Paper-2) | | | | |
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| | est Type Timing | | | | |
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| | HT-1 | | | HT-2 | |
| Heat Transfer | Steady and unsteady heat condu Radiative heat transfer | | Free and force | d convection, boiling and condensation, Heat exchanger. | |
| | ICE-1 | | | ICE-2 | |
| IC Engines | SI and CI Engines, Engine Systems and (| Components, Fuels. | | naracteristics and testing of IC Engines; ssion Control. Otto, Diesel and Dual Cycles. | |
| | RAC-1 | | | RAC-2 | |
| Refrigeration Air Conditioning | Vapour compression refrigeration, Compressors, Other types of refrigeration Absorption, Vapour jet, thermo electric refrigeration and Heat pu | systems like Vapour and Vortex tube | Comfort and indus | roperties and processes, Comfort chart, trial air conditioning, Load calculations and Evaporators and Expansion devices. | |
| | FMM-1 | FM | M-2 | FMM-3 | |
| Fluid Mechanics and Machinery | Basic Concepts and Properties of Fluids, Manometry, Fluid Statics, Buoyancy, Equations of Motion such as velocity potential, Stream Function. | Viscous flow of inc Laminar and Turbule | n and applications, compressible fluids, nt flows, Flow through l losses in pipes. | Reciprocating and Centrifugal pumps, Hydraulic Turbines and other hydraulic machines. | |
| | PPE-1 | PP | PE-2 | PPE-3 | |
| Power Plant Engineering | Steam and Gas Turbines, Rankine and Brayton cycles with regeneration and reheat. | analysis, Theory Pulse jet and R | roperties, Flue gas of Jet Propulsion – am Jet Engines, Rotary Compressors. | Boilers, power plant components like condensers, air ejectors, Electrostatic precipitators and cooling towers. | |
| | RSE-1 | | | RSE-2 | |
| Renewable Sources of Energy | Solar Radiation, Solar Thermal Energy collection - Flat Plate andfocusing collectors their materials and performance. Solar Thermal Energy Storage, Applications – heating, cooling and Power Generation. | | Solar Photovoltaic Conversion; Harnessing of Wind Energy, Bio-mass and Tidal Energy – Methods and Applications, Working principles of Fuel Cells. | | |
| Engineering | Mech-1 | Me | ch-2 | Mech-3 | |
| Mechanics (SoM) | Analysis of System of Forces, Friction, Centroid and Centre of Gravity, Dynamics. | and Strains, Ben | -Compound Stresses ding Moment and e Diagrams. | Theory of Bending Stresses-Slope and deflection-Torsion, Thin and thick Cylinders, Spheres. | |
| | MS-1 | | | MS-2 | |
| Engineering Materials | Basic Crystallography, Alloys and Phase diagrams, Heat Treatment. | | Ferrous and Non Ferrous Metals, Non metallic materials, Basics of Nano-materials, Mechanical Properties and Testing, Corrosion prevention and control. | | |
| | ToM-1 | То | M-2 | ToM-3 | |
| Mechanisms and Machines | Mechanisms, Kinematic Analysis, Velocity and Acceleration. CAMs with uniform acceleration, cycloidal motion, oscillatingfollowers; Effect of Gyroscopiccouple on automobiles, ships and aircrafts. Governors. | of undamped an systems, Transmiss | and forced vibration d damped SDOF ibility Ratio, Vibration Speed of Shafts. | Geometry of tooth profiles, Law of gearing, Interference, Helical, Spiral and Worm Gears, Gear Trains- Simple, compound and Epicyclic. Slider crank mechanisms, Balancing. | |
| | MD-1 | | | MD-2 | |
| Design of Machine Elements | Design for static and dynamic loading; failure theories; fatigue strength and the S-N diagram; principles of the design of machine elements such as riveted, welded and bolted joints. | | | ars, rolling and sliding contact bearings, kes and clutches, flywheels. | |
| | PROD-1 | IE | -1 | RE-1 | |
| Manufacturing, Industrial and | Metal casting-Metal forming, Metal Joining, computer Integrated manufacturing, FMS. | Inventor | ning and Control, ry control | Failure concepts and characteristics- Reliability, Failure analysis, Machine Vibration, Data acquisition, Fault Detection, Vibration Monitoring. | |
| Maintenance | PROD-2 | IE | -2 | RE-2 | |
| Engineering | Machining and machine tool operations, Limits, fits and tolerances, Metrology and inspection. | Operations resea | arch - CPM-PERT | Field Balancing of Rotors, Noise Monitoring, Wear and Debris Analysis, Signature Analysis, NDT Techniques in Condition Monitoring. | |
| | MR-1 | | | MR-2 | |
| Mechatronics and Robotics | Microprocessors and Micro controllers: Architecture, programming, I/O,Computer interfacing, Programmable logic controller. Sensors and actuators, Piezoelectric accelerometer, Hall effect sensor, Optical Encoder, Resolver, Inductosyn, Pneumatic and Hydraulic actuators, stepper motor, Control Systems- Mathematical modeling of Physicalsystems, control signals, controllability and observability | | Robotics, Robot Classification, Robot Specification, notation; Direct and Inverse Kinematics; Homogeneous Coordinates and Arm Equation of four Axis SCARA Robot. | | |

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(d) S + 2π

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Ans. (b)

(c) $\frac{2\pi}{S}$

Sol. For cylinder motions the circumference of rolling circle is equal to stroke i.e. follower displacement. Hence

 $2\pi r = S$

- \therefore Radius of rolling circle r = S/2 π
- **39.** A vertical shaft of 100 mm diameter and 1 m length has its upper end fixed at the top. The other end carries a disc of 5000 N and the modulus of elasticity of the shaft material is 2×10^5 N/mm². Neglecting of the longitudinal vibrations will be nearly

| (a) 279.5 Hz (b) 266.5 Hz | (a) 279.5 Hz | (b) 266.5 Hz |
|---------------------------|--------------|--------------|
|---------------------------|--------------|--------------|

(c) 253.5 Hz (d) 241.5 Hz

Ans. (a)

Sol. The extension in vertical shaft is calculated by stress equation



: Extension in shaft,

$$\delta = \frac{\sigma \ell}{\mathsf{E}} = \frac{\mathsf{w}\ell}{\mathsf{A}\mathsf{E}}$$

The frequency of longitudinal vibration,

$$f = \frac{1}{2\pi} \sqrt{\frac{g}{\delta}} = \frac{1}{2\pi} \sqrt{\frac{gAE}{w\ell}}$$
$$= \frac{1}{2\pi} \sqrt{\frac{9.81 \times \frac{\pi}{4} \cdot 100^2 \times 2 \times 10^5}{5000 \times 1.0}}$$

= 279.4 Hz

40. The accurate method of finding the natural frequency of transverse vibration of a system of several loads attached to some shaft is

- (a) Dunkerley method
- (b) energy method
- (c) Stodola method
- (d) Dunkerley and energy method

Ans. (b)

Sol. Dunkerley method, Stodola method and Holzar's methods are numerical methods but approximate. Energy method gives accurate frequency.

41. The speed at which the shaft runs, so that the deflection of the shaft from the axis of rotation becomes infinite, is known as

- (a) whipping speed
- (b) damping speed
- (c) resonant speed
- (d) gravitational speed

Ans. (a)

- **42.** Which one of the following is not the correct statement with respect to the involute profile toothed gears in mesh?
 - (a) Pressure angle remains constant from the start till the end of the engagement.
 - (b) The base circle diameter and the pitch circle diameter of the two mating involutes are proportional.
 - (c) When two involutes are in mesh, the angular velocity ratio is proportional to the size of the base circles.
 - (d) The shape of the involute profile depends only on the dimensions of the base circle.

Ans. (c)

43. The centre distance C between two gears, in terms of base circle radii R_1 , R_2 and the pressure angle ϕ , is





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(a)
$$\frac{\cos\phi}{R_1 + R_2}$$
 (b) $\frac{R_1 + R_2}{\cos\phi}$
(c) $\left(\frac{R_1}{R_2}\right) \cdot \cos\phi$ (d) $\left(\frac{R_2}{R_1}\right) \cdot \cos\phi$

Ans. (b)

Sol. The centre distance between two gears,

C = Sum of pitch circle radii

$$= r_1 + r_2$$
$$\frac{R_1}{\cos\phi} + \frac{R_2}{\cos\phi} = \frac{(R_1 + R_2)}{\cos\phi}$$

44. A three-cylinder single-acting engine has its cranks at 120°. The turning moment diagram for each cycle is a triangle for the power stroke with a maximum torque of 60 Nm at 60° after the dead centre of the corresponding crank. There is no torque on the return stroke. The engine runs at 400 r.p.m. the power developed will be

| (a) | 1745 W | (b) 1885 W | |
|-----|--------|------------|--|
| (c) | 1935 W | (d) 1995 W | |

Ans. (b)

Sol. The turning moment diagram.



 $T_m = \overline{\text{crank angle}}$

$=\frac{90\,\pi}{2\pi}=45$ N-m

Power developed,

$$\mathsf{P} = \mathsf{T}_{\mathsf{m}} \cdot \boldsymbol{\omega} = 45 \times \frac{2\pi \times 400}{60}$$

45. A vertical single-cylinder opposed piston type engine has reciprocating parts of mass 2000 kg for the lower piston and 2750 kg for the upper piston. The lower piston has a stroke of 60 cm and the engine is in primary balance. If the ratio of the length of connecting rod to crank is 4 for the lower piston and 8 for the upper piston, and when the crankshaft speed is of 135 r.p.m., the maximum secondary unbalanced force will be

Ans. (c)

Sol. Since the engine is in complete primary balance,



- $\therefore \quad \mathbf{m}_1 \mathbf{r}_1 \pm \mathbf{m}_2 \mathbf{r}_2 = \mathbf{0}$
- ... Radius or crank length of upper piston

$$r_1 = \frac{m_2 r_2}{m_1} = \frac{2000 \times 30}{2750} = 21.82 \text{cm}$$

... Maximum secondary force

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- Sol. Note: Assuming extra 'C' outside bracket as misprint
- The active gyroscopic torque in gyroscope 47. about a horizontal axis represents
 - (a) the torque required to cause the axis of spin to precess in the vertical plane
 - (b) the torque required to cause the axis of spin to precess in the horizontal plane
 - (c) the force required to cause the axis of spin to precess in the horizontal plane
 - (d) the force required to cause the axis of spin to precess in the vertical plane

Ans. (b)

48. The change in governor height for a Watt governor when speed varies from 100 r.p.m. to 101 r.p.m. will be nearly

(a) 1.8 mm (b) 2.6 mm (c) 3.4 mm

(d) 4.2 mm

Ans. (a)

Sol. Height of Watt governor,

$$H = \frac{895000}{N^2} mm$$
 ...(i)

where, N is rpm

$$H_1 = \frac{89500}{100^2} = 89.5 \,\mathrm{mr}$$

At N = 101 rpm

$$H_2 = \frac{895000}{101^2} = 87.74 \text{ mm}$$

- Change in height, ÷
 - $\Delta H = H_1 H_2 = 89.5 87.74 = 1.76$ mm
- 49. A rectangular strut is 150 mm wide and 120 mm thick. It carries a load of 180 kN at an eccentricity of 10 mm in a plane bisecting the thickness as shown in the figure



The maximum intensity of stress in the section will be

- (a) 14 MPa (b) 12 MPa
- (c) 10 MPa (a)

(d) 8 MPa

Ans.

Sol. Maximum intensity of stress = $\sigma_{b} + \sigma_{c}$





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$$= \frac{My}{I} + \frac{P}{A}$$

= $\frac{180 \times 10^3 \times 10 \times 75}{\frac{120 \times 150^3}{12}} + \frac{180 \times 10^3}{12 \times 150}$
= 4 + 10
= 14 MPa

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- **50.** The theory of failure used in designing the ductile materials in a most accurate way is by
 - (1) maximum principal stress theory
 - (2) distortion energy theory
 - (3) maximum strain theory

Select the correct answer using the code given below.

| (a) 1, 2 and 3 | (b) 1 only |
|----------------|------------|
|----------------|------------|

(c) 2 only (d) 3 only

Ans. (c)

- **Sol.** The most accurate way of designing ductile material is by use of distortion energy theory or Von-mises theory.
- **51.** When a load of 20 kN is gradually applied at a particular point in a beam, it produces a maximum bending stress of 20 MPa and a deflection of 10 mm. What will be the height from which a load of 5 kN should fall onto the beam at the same point if the maximum bending stress is 40 MPa?

| (a) | 80 | mm | | | (b) | 70 mm |
|-----|----|----|--|--|-----|-------|
|-----|----|----|--|--|-----|-------|

- (c) 60 mm (d) 50 mm
- Ans. (c)
- Sol. Given, For 20 KN static load

$$\delta = 10 \text{ mm}$$

 $\sigma_{\text{static1}} = 20 \text{ MPa}$

For 5 KN impact load

 $\sigma_{max} = 40 \text{ MPa}$

For this $\sigma_{\text{static2}} = ?$

as
$$\sigma = \frac{My}{I} = \sigma \times P$$

$$\Rightarrow \frac{\sigma_{\text{static 2}}}{\sigma_{\text{static 1}}} = \frac{5}{20}$$

$$\Rightarrow \sigma_{\text{static 2}} = 5$$

Calculation of $\,\delta_{st}\,$ as $\,\delta_{st}\,\propto {\sf P}$

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Engineering

$$\Rightarrow \frac{\delta_{st}}{10} = \frac{s}{20}$$

 $\Rightarrow \delta_{st}$ =2.5

As we know for impact load,

$$\sigma_{\text{max}} = \sigma_{\text{st}} \left(1 + \sqrt{1 + \frac{2h}{\delta_{\text{st}}}} \right)$$

$$\Rightarrow \frac{40}{5} = \left(1 + \sqrt{1 + \frac{2h}{2.5}} \right)$$

$$\Rightarrow 8 = 1 + \sqrt{1 + \frac{2h}{2.5}}$$

$$\Rightarrow 7^2 - 1 = \frac{2h}{2.5}$$

$$48 = \frac{2h}{2.5}$$

$$\boxed{h = 60 \text{ mm}}$$

- **52.** The areas of fatigue failure in a part may be in the
 - (1) region having slow growth of crack with a fine fibrous appearance.
 - (2) region having faster growth of crack with a fine fibrous appearance.
 - (3) region of sudden fracture with a coarse granular appearance.
 - (4) region of gradual fracture with a coarse granular appearance.

Select the correct answer using the code given below.

SCROLL DOWN

| (a) 2 and 3 | (b) 2 and 4 |
|-------------|-------------|
| | |

(c) 1 and 4 (d) 1 and 3



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Ans. (d)

- Sol. The slow growth of crack in fatigue failure • results in fine fibrous appearance i.e. smooth and polished surface. Basically it occures in initial stage.
 - In the later stage, the fracture is sudden without warning and appearance of this portion of surface in coarse granular as shown in figure



surface (later stage)

- 53. The shock-absorbing capacity (resilence) of bolts can be increased by
 - (a) increasing the shank diameter above the core diameter of threads
 - (b) reducing the shank diameter to the core diameter of threads
 - (c) decreasing the length of shank portion of the bolt
 - (d) pre-heating of the shank portion of the bolt

Ans. (b)

- Sol. The shock absorbing capacity of a bolt can increased by reducing the diameter of unthreaded part. This can be done either by reducing diameter of unthreaded part or making hole in unthreaded part along axis. This concept is used in bolt of uniform strength.
- 54. The torque required to tighten the bolt comprises of the
 - (a) torque required in overcoming thread friction only
 - (b) torque required in inducing the pre-load only
 - (c) torque required in overcoming

circumferential hoop stress

(d) torque required in overcoming thread friction and inducing the pre-load and also the torque required to overcome collar friction between the nut and the washer

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- Ans. (d)
- 55. A steel spindle transmits 4 kW at 800 r.p.m. The angular deflection should not exceed 0.25°/m length of the spindle. If the modulus of rigidity for the material of the spindle is 84 GPa, the diameter of the spindle will be
 - (a) 46 mm (b) 42 mm

(d) 34 mm (c) 38 mm

60

(d) Ans.

Sol. Power, P =
$$\frac{2\pi NT}{60}$$

$$\Rightarrow$$
 Torque, T = $\frac{60P}{2\pi N}$

$$= \frac{60 \times 4 \times 10^3}{2\pi \times 800} = 47.746 \text{ N-m}$$

Angular deflection, $\theta = \frac{T\ell}{JG} = \frac{T\ell}{\frac{\pi d^4}{2\Omega} \cdot G}$

$$\frac{\pi}{180} \times 0.25 = \frac{47.746 \times 1 \times 32}{\pi \times d^4 \times 84 \times 10^9}$$

$$\therefore d = 33.9 \text{ mm} \approx 34 \text{ mm}$$

56. A taper roller bearing has a dynamic load capacity of 26 kN. The desired life for 90% of the bearings is 8000 hr and the speed is 300 r.p.m. The equivalent radial load that the bearing can carry will be nearly

| (a) 5854 N (b) | 5645 N | |
|----------------|--------|--|
|----------------|--------|--|

(c) 5436 N (d) 5227 N

Ans. (a)

Sol. Life of bearing in millions of revolutions,

$$40 = \frac{60 \text{ NL}_{10h}}{10^6} = \frac{60 \times 300 \times 8000}{10^6}$$



= 144 million rev.

Equivalent radial load,

$$L = \left(\frac{C}{P}\right)^{10/3} \times 10^{6}$$
$$P = \frac{C}{(144)^{0.3}} = \frac{26000}{(144)^{0.3}} = 5854 \text{ N}$$

- **57.** Hollow shafts are stronger than solid shafts having same weight because
 - (a) the stiffness of hollow shaft is less than that of solid shaft

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- (b) the strength of hollow shaft is more than that of solid shaft
- (c) the natural frequency of hollow shaft is less than that of solid shaft
- (d) in hollow shafts, material is not spread at large radius

Ans. (b)

- **Sol.** Strength (polar modulus) of hollow shaft is more than that of solid shaft.
- **58.** A propeller shaft is required to transmit 45 kW power at 500 r.p.m. It is a hollow shaft having inside diameter 0.6 times the outside diameter. It is made of plain carbon steel and the permissible shear stress is 84 N/mm². The inner and outer diameters of the shaft are nearly.
 - (a) 21.7 mm and 39.1 mm
 - (b) 23.5 mm and 39.1 mm
 - (c) 21.7 mm and 32.2 mm
 - (d) 23.5 mm and 32.2 mm

Ans. (b)

Sol. $D_i = 0.6 D_o$

Power, P =
$$\frac{2\pi NT}{60}$$

45 × 10³ = $\frac{2\pi \times 500 \times T}{60}$

∴ Torque, T = 859.466 Nm

Permissible stress, $\sigma = \frac{\text{Tr}}{1}$

$$= \frac{T \times \frac{D_o}{2}}{\frac{\pi}{32} (D_0^4 - D_i^4)} = \frac{16T}{\pi D_o^3 \left[1 - \left(\frac{D_i}{D_o}\right)^4 \right]}$$

$$84 = \frac{16 \times 859.466 \times 10^3}{\pi D_o^3 \left[1 - (0.6)^4 \right]}$$

$$D_o = 39.1 \text{ mm}$$

$$\therefore \quad D_i = 0.6 \text{ } D_o = 23.47 \text{ mm}$$

59. A bicycle and rider travelling at 12 km/hr on a level road have a mass of 105 kg. A brake is applied to a rear wheel having 800 mm diameter. The pressure on the brake is 80 N and the coefficient of friction is 0.06. The number of turns of the wheel before coming to rest will be

- (a) 48.3 revolutions (b) 42.6 revolutions
- (c) 38.3 revolutions (d) 32.6 revolutions

Ans. (a)

Sol. Assuming the bicycle and rider as a ring, the moment of inertia.

 $I = mr^2 = 105 \times 0.4^2 = 16.8 \text{ kg-m}^2$

Initial angular velocity of disc

$$\omega = \frac{V}{r} = \frac{12 \times 5}{18 \times 0.4} = \frac{25}{3} \text{ rad/sec.}$$

The friction force on whirl,

 $f = \mu P = 0.06 \times 80 = 4.8N$

The torque due to brake

 $\tau = r.f = 0.4 \times 4.8 = 1.42 \text{ N-m}$

The angular acceleration, $\alpha = \frac{\tau}{r}$

 $= \frac{192}{168} = 0.1143 \text{ rad/sec}^2$

From equation of motion,

 $\omega_{\rm f}^2 = \omega_{\rm i}^2 - 2\alpha\theta$

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 $0 = \omega^2 - 2\alpha\theta$

Angular displacement during braking

$$\theta = \frac{\omega^2}{2\alpha} = \frac{(25/3)}{2 \times 0.1143}$$

= 303.8 radians

Numbers of revolutions during braking

n =
$$\frac{\theta}{2\pi} = \frac{303.8}{2\pi}$$
 = 48.35 rev.

- **60.** To avoid self-engagement in cone clutch, its semi-cone angle is always kept
 - (a) smaller than the angle of static friction
 - (b) equal to the angle of static friction
 - (c) greater than the angle of static friction
 - (d) half of the angle of static friction

Ans. (c)

61. In case of arc welding of steel with a potential of 20 V and current of 200 A, the travel speed is 5 mm/s and the cross-sectional area of the joint is 20 mm². The heat required for melting steel may be taken as 10 J/mm³ and heat transfer efficiency as 0.85. The melting efficiency will be nearly

| (a) 18% | (b) 29% |
|----------|----------|
| (a) 1070 | (0) 2370 |

(c) 36% (d) 42%

Ans. (b)

Sol. Voltage, V = 20V

Current, I = 200A

Welding speed, v = 5 mm/s Cross-sectional area, A = 20 mm² Heat required to melt steel = 10J/mm³ = H_m

Heat transfer efficiency, $\eta_{th} = 0.85$

Melting efficiency, $\eta_m = ?$

$$\eta_{m} = \frac{H_{m}}{H_{2}} = \frac{10}{\frac{VI}{A \times v} \times \eta_{HT}}$$

 $= \frac{10}{\frac{20 \times 200}{20 \times 5} \times 0.85} = 0.294$

 $\eta_m = 29.4\%$

62. What is the force required for 90° bending of St50 steel of 2 mm thickness in a V-die, if the die opening is taken as 8 times the thickness and the length of the bent part is 1 m, ultimate tensile strength is 500 MPa and K = 1.33?

(a) 166.25 kN (b) 155.45 kN

(c) 154.65 kN (d) 143.85 kN

Ans. (a)

Sol. Ultimate tensile strength, UTS = 500 MPa

Thickness, t = 2mm

Length of bent part, L = 1m

Width of die opening, $W = 8 \times \text{thickness} = 8 \times 2 = 16 \text{ mm}$

Fadal K = 1.33 for V-die

K = 0.3 to 0.34 for wiping die

Bending force, F = K×UTS× $\frac{L}{W}$ ×t²

$$\mathsf{F} = \frac{1.33 \times 500 \times (1 \times 10^3) \times 2^2}{16}$$

= 16,6250 N

- = 166.25 KN
- **63.** A graph is drawn to a vertical magnification of 10000 and horizontal magnification of 100, and the areas above and below the datum line are as follows:

| Above | 150 mm ² | 80 mm ² | 170 mm ² | 40 mm ² |
|-------|---------------------|--------------------|---------------------|---------------------|
| Below | 80 mm ² | 60 mm ² | 150 mm ² | 120 mm ² |

The average roughness Ra for sampling length of 0.8 mm will be

| (a) 1.14 μm | (b) 1.10 μm |
|-------------|-------------|
| (c) 1.06 μm | (d) 1.02 μm |

Ans. (c)





| Sol. | Vertical magnification, VM = 10,000 | |
|--------|---|----|
| | Horizontal magnification, HM = 100 | |
| | Sum of areas above & below datum line, | |
| | $\Sigma A = 150 + 80 + 170 + 40 + 80 + 60 + 150$ + 120 = 850 mm ² | |
| | Sampling length, L = 0.8 mm | |
| | Average roughness, | 4 |
| | $R_{a} = \frac{\Sigma A}{L} \times \frac{1}{\text{vertical scale}} \times \frac{1}{\text{horizontal scale}}$ | : |
| | $R_{a} = \frac{\Sigma A}{L} \times \frac{1}{10^{4}} \times \frac{1}{10^{2}} \text{ mm}$ | |
| | $= \frac{850}{0.8} \times \frac{1}{10^6} \mathrm{mm}$ | |
| | R _a = 1.06 μm | |
| 64. | The radius of arc is measured by allowing a 20 mm diameter roller to oscillate to and fro on it and the time for 25 oscillations is noted at 56.25 s. The radius of arc will be | |
| | (a) 865 mm (b) 850 mm | |
| | (c) 835 mm (d) 820 mm | |
| Ans. | (b) | 4 |
| Sol. | Radius of roller, $r = \frac{20}{2} = 10 \text{ mm}$ | : |
| | Time period of oscillation, T = $\frac{56.25}{25}$ | |
| | = 2.25 sec. | |
| | Acceleration due to gravity, $g = 9.81 \text{ m/s}^2$ = 9810 mm/s ² | |
| | Radius of arc, R = $\frac{T^2 \times g}{6\pi^2}$ + r | |
| | $R = \frac{(2.25)^2 \times 9810}{6 \times \pi^2} + 10 = 848.65 \text{ mm}$ | |
| | R = 848.65 mm | |
| 65. | Which one of the following systems is consisting of processing stations, material | |
| | | |
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handling and storage, computer control system and human labour? (a) Portable manufacturing system (b) Focused integrated system (c) Flexible manufacturing system (d) Automated integrated system Ans. (c) Sol. Flexible manufacturing system (FMS) consists of a group of NC machines connected together by an automated material handling system and operating under computer control. The basic components of FMS are machine tools and the related equipment; material handling equipment; computer control system and the human labour. A project initially costs Rs 5,000 and generates 66. year-end cash inflows of Rs 1,800, Rs 1,600, Rs 1,400, Rs 1,200 and Rs 1,000 respectively in five years of its life. If the rate of return is 10%, the net present value (NPV) will be (a) Rs 500 (b) Rs 450 (c) Rs 400 (d) Rs 350 Ans. (b) **Sol.** NPV = $\left[\frac{1800}{1.1} + \frac{1600}{1.1^2} + \frac{1400}{1.1^3} + \frac{1200}{1.1^4}\right]$ $+\frac{1000}{1.1^5}$ -5000 [1636.36 + 1322.31 + 1051.84 + 819.62 + 620.92] = 451 67. What is the mode for the following distribution? Gross profit as Number of

| Giuss piùni as | |
|---------------------|-----------|
| percentage of sales | companies |
| 0-7 | 19 |
| 7 – 14 | 25 |
| 14-21 | 36 |
| 21-28 | 72 |
| 28 - 35 | 51 |
| 35 – 42 | 43 |
| 42 – 49 | 28 |
| | |

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|--------------|--|-------------|---|
| Ans. Sol. | (a) 19.55 (b) 21.40 (c) 23.25 (d) 25.10 (d) Mode = $L + \left[\frac{(f_m - f_{m-1})}{(f_m - f_{m-1}) + (f_m - f_{m+1})} \right] \times w$ | Sol. | R(t) = $e^{-\lambda t}$ Given, R(t) = 0.8 for t = 2 × 10 ³ hr ∴ $\lambda = -0.5 × 10-3 Ln(0.8)$ = 1.12 × 10 ⁻⁴ /hr |
| | $= 21 + \frac{(72 - 36)}{(72 - 36) + (72 - 51)} \times 7$ $= 21 + \frac{36}{36 + 21} \times 7$ $= 25.42$ | | Steady state availability, $0.98 = \frac{\mu}{\mu + \lambda}$ $\Rightarrow \mu = 0.98\mu + 1.12 \times 10^{-4} \times 0.98$ $\Rightarrow \mu = 5.49 \times 10^{-3}/hr$ 1 10 ³ |
| 68. | Consider the following data for quality acceptance process: N = 10000 n = 89 c = 2 p = 0.01 (incoming lots of quality) $P_a = 0.9397$ The AOQ will be | 70. Ans. | $\therefore \text{ MTTR} = \frac{1}{\mu} = \frac{10^3}{5.49} = 182.2 \text{ hrs}$ Which one of the following relations with usual notations will hold good in a dynamic vibration absorber system under tuned conditions? (a) $k_1k_2 = m_1m_2$ (b) $k_1m_2 = m_1k_2$ (c) $k_1m_1 = k_2m_2$ (d) $k_1 + k_2 = m_1 + m_2$ (b) |
| Ans. Sol. | (a) 0.93% (b) 0.84% (c) 0.75% (d) 0.66% (a) $AOQ = \frac{(N-n)Pa \cdot p}{N}$ | 71. | In ultrasonic waves, the frequencies for non- destructive testing of materials are in the range of (a) 0.5 MHz to 10 MHz |
| 501 | $= \frac{(10000 - 89) \times 0.9397 \times 0.01}{10000}$ = 0.0093 or 0.93% | Ans. | (b) 10 MHz to 20 MHz (c) 20 MHz to 30 MHz (d) 30 MHz to 40 MHz (a) |
| 69. | An engine is to be designed to have a minimum reliability of 0.8 and minimum availability of 0.98 over a period of 2×10^3 hr. The MTTR is nearly (a) 168 hr (b) 174 hr | 72. Ans. | The Curie point for most ferrous magnetic materials is about (a) 390 °C (b) 540 °C (c) 760 °C (d) 880 °C (c) |
| Ans. | (c) 183 hr (d) 188 hr (c) | 73. | Which of the following is one of the basic units of memory controller in micro-controller? 3406, Mobile: 8130909220, 9711853908 |



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- (a) Microcode engine
- (b) Master program counter
- (c) Program status word
- (d) Slave program counter
- Ans. (d)
- **74.** Which one of the following ways will be adopted to store the program counter contents?
 - (a) Last-in-First-out (LIFO)
 - (b) First-in-First-out (FIFO)
 - (c) Last-in-Last-out (LILO)
 - (d) First-in-Last-out (FILO)

Ans. (a)

- **75.** In ladder logic programming, an alternative in place of using same internal relay contact for every rung is to use
 - (a) battery-backed relay
 - (b) dummy relay
 - (c) one-shot operation
 - (d) master control relay

Ans. (d)

- **Sol.** A whole block of outputs can be simultaneously turned off or on by using the some internal relay contacts in each output rung so that switching it on or off affects every one of the rungs. An alternative way of programming to achieve the some effect is to use a master relay.
- 76. Consider the following statements:
 - (1) The term 'attenuation' is used to describe the process of removing a certain band of frequencies from a signal and permitting others to be transmitted.
 - (2) The Wheatstone bridge can be used to convert a voltage change to an electrical resistance change.



| (a) 1 only | (b) 2 only |
|------------------|-----------------|
| (a) Dath 1 and 0 | (d) No:ther 1 o |

(c) Both 1 and 2 (d) Neither 1 and 2

Ans. (d)

Sol. The wheat stone bridge can be used to convert a resistance change to a voltage change.

The term 'filtering' is used to describe the process of removing a certain band of frequencies from a signal and permitting others to be transmitted.

- **77.** At time t, the excitation voltage to a resolver is 24 V. The shaft angle is 90°. The output signals from the resolver V_{S1} and V_{S2} will be
 - (a) 12 V and 0 V (b) 24 V and 0 V
 - (c) 12 V and 12 V (d) 24 V and 12 V

Ans. (b)

- Sol. Output signals of resolver are
 - $V_{s1} = V_1 \sin \alpha$
 - $V_{s2} = V_1 \cos \alpha$

for $~\alpha=90^\circ$,

- $V_{s1} = 24V$ and $V_{s2} = 0V$
- **78.** An actuator having a stem movement at full travel of 30 mm is mounted with a control valve having an equal percentage plug and with minimum flow rate of 2 m³/s and maximum flow rate of 24 m³/s. When the stem movement is 10 mm, the flow rate will be
 - (a) $3.4 \text{ m}^3/\text{s}$ (b) $3.8 \text{ m}^3/\text{s}$

Ans. (d)

$$\frac{Q}{Q_{min}} = \left(\frac{Q_{max}}{Q_{min}}\right)^{\left(\frac{S-S_{min}}{S_{max}-S_{min}}\right)}$$

For
$$Q_{min} = 2m^3/s$$

$$\frac{Q}{2} = \left(\frac{24}{2}\right)^{\left(\frac{10-0}{30-0}\right)}$$

Q = 4.57 m³/s



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- **79.** In a rack and pinion system, rack is an element moving in translational direction and pinion is a rotary gear. Which one of the following statements is correct?
 - (a) Translational acceleration is directly proportional to the moment of inertia of pinion.
 - (b) Translational acceleration is inversely proportional to the moment of inertia of pinion.
 - (c) Angular acceleration is inversely proportional to the torque on pinion shaft.
 - (d) Translational velocity is directly proportional to the moment of inertia of pinion.

Ans. (b)

- **Sol.** Translation acceleration, $a_t = r \times \alpha$
 - $\alpha = \frac{T}{I}$ so, $a_t = \frac{Tr}{I}$

 \mathbf{a}_{t} is inversely proportional to the moment of inertia.

- **80.** For the control signal to change at a rate proportional to the error signal, the robotic controller must employ
 - (a) integral control
 - (b) proportional-plus-integral control
 - (c) proportional-plus-derivative control
 - (d) proportional-plus-integral-plus-derivative control

Ans. (a)

81. What is the minimum number of degrees of freedom that a robot needs to have in order to locate its end effectors at an arbitrary point with an arbitrary orientation in space?

| Ans. | (d) | | |
|------|-------|----|------|
| | (c) 5 | (0 | d) 6 |
| | (a) 3 | (k | o) 4 |

Engineering Using a robot with 1 degree of freedom and having 1 sliding joint with a full range of 1 m, if the robot's control memory has a 12-bit storage capacity, the control resolution for the

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(a) 0.236 mm (b) 0.244 mm

(c) 0.252 mm (d) 0.260 mm

Ans. (b)

82.

Sol. control resolution = $\frac{\text{stroke length}}{2^n}$

axis of motion will be

here, stroke length = 1000 mm

C.R. =
$$\frac{1000}{2^{12}}$$
 = 0.244 mm

- 83. Assume that the joint mechanisms at serial link manipulators are frictionless. The joint torque τ required to bear an arbitrary end point force F is
 - (a) J⁻¹F (b) JF
 - (c) $J^T F$ (d) $J^{-1} F^T$

Ans. (c)

- Sol. For an n degree of freedom, serial link robot having no friction at the joints, the joint torques τ, that are required to bear an arbitrary end point force, F is
 - $\tau = J^T \cdot F$
- 84. Rotate the vector v = 5i + 3j + 8k by an angle of 90° about the x-axis. The rotated vector (Hv) would be





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Sol.
$$R_{x} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos 90^{\circ} & -\sin 90^{\circ} \\ 0 & \sin 90^{\circ} & \cos 90^{\circ} \end{bmatrix}$$
$$Hv = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} 5 \\ 3 \\ 8 \end{bmatrix}$$
$$= \begin{bmatrix} 5+0+0 \\ 0+0-8 \\ 0+3+0 \end{bmatrix} = \begin{bmatrix} 5 \\ -8 \\ 3 \end{bmatrix}$$

Directions:

Each of the six (6) items consists of two statements, one labelled as 'Statement (I)' and the other as 'Statement (II)'. You are to examine these two statements carefully and select the answers to these items using the code given below:

Code:

- (a) Both Statement (I) and Statement (II) are individually true and Statement (II) is the correct explanation of Statement (I)
- (b) Both Statement (I) and Statement (II) are individually true but Statement (II) is **not** the correct explanation of Statement (I)
- (c) Statement (I) is true but Statement (II) is false
- (d) Statement (I) is false but Statement (II) is true
- **85. Statement (I):** The function of arithmetic logic unit (ALU) in microprocessor is to perform data manipulation.

Statement (II): The status register is where data for an input to the arithmetic and logic unit is temporarily stored.

Ans. (d)

86. Statement (I): To use a sensor, we generally need to add signal conditioning circuitry, such as circuits which amplify and convert from analog to digital, to get the sensor signal in the right form, take account of any non-linearities, and calibrate it.

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Statement (II): A smart sensor is integrated with the required buffering and conditioning circuitry in a single element and provides functions beyond that of just a sensor.

Ans. (b)

87. Statement (I): The count-up overflow (OV) bit is 1 when the up-counter increments above the maximum positive value.

Statement (II): The count-down underflow (UN) bit is 1 when the counter decrements below the minimum negative value.

Ans. (c)

- **Sol.** The count-down underflow (UN) bit is 1 when the counter decrements below the maximum negative value.
- **88.** Statement (I): The multiplexer is essentially an electronic switching device which enables each of the inputs to be sampled in turn.

Statement (II): A multiplexer is a circuit that is able to have inputs of data from a number of sources and then, by selecting an input channel, gives an output from just one of them.

- Ans. (a)
- **89. Statement (I):** The term 'encoder' is used for a device that provides an analog output as a result of angular or linear displacement.

Statement (II): An increment encoder detects changes in angular or linear displacement from some datum position where as an absolute encoder gives the actual angular or linear position.

Ans. (d)

- **Sol.** An encoder is a device that provides a digital output in response to a linear or angular displacement.
- **90. Statement (I):** Process control valves are used to control the rate of fluid flow and are used where, perhaps, the rate of flow of a liquid into a tank has to be controlled.





Statement (II): A common form of pneumatic actuator used with process control valves is the diaphragm actuator.

- Ans. (b)
- 91. The solar heat pipe works on the principle of
 - (a) heating and condensation cycle
 - (b) evaporation and condensation cycle
 - (c) coolilng and condensation cycle
 - (d) heating and evaporation cycle
- Ans. (b)
- **Sol.** When the solar radiation falls on the fin tube heat pipe, heat is absored and transmitted to the working fluid in the heat pipe.



- **92.** A good approximation of the measured solar spectrum is made by
 - (a) black-body energy distribution
 - (b) Planck's energy distribution
 - (c) inverse square law
 - (d) solar constant
- Ans. (a)
- **Sol.** The spectrum of the sun's solar radiation close to that of black body with a temperature about 5800K.
- **93.** Which one of the following types of tracker uses liquid contained in canisters that can turn easily into vapour?
 - (a) Active tracker
 - (b) Passive tracker
 - (c) Single-axis tracker
 - (d) Altitude-azimuth tracker

Ans. (b)

Sol. Passive trackers use the heat from sunlight to vapourize liquid Freon contained in cansisters mounted on the tracker.

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- **94.** Which type of flat-plate collector is used to heat the swimming pools with plastic panel, utilizing solar energy?
 - (a) Pipe and fin type
 - (b) Full water sandwich type
 - (c) Thermal traps type
 - (d) Corrugated plate with selective surface type

Ans. (b)

95.

Sol. Full water sandwich type are used where both the wetted area and the water capacity are high e.g. swimming pool.

The edge loss U_e in a solar collector with respect to edge area A_e , collector area A_c and back loss coefficient U_b is

a)
$$U_{b}\left(\frac{A_{e}}{A_{c}}\right)$$
 (b) $U_{b}\left(\frac{A_{c}}{A_{e}}\right)$
c) $A_{c}\left(\frac{A_{e}}{U_{b}}\right)$ (d) $U_{b}\left(\frac{A_{e}}{2A_{c}}\right)$

Ans. (a)

(

(

Sol.



- **96.** In solar porous type air heater, the pressure drop is usually
 - (a) higher than non-porous type
 - (b) same as in non-porous type
 - (c) lower than non-porous type
 - (d) zero

Ans. (a)

Sol. Pressure drop increases with an increase in porous layer.



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97. In a drainback solar water heating system

(a) the water in the heat exchanger is recycled

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- (b) the water is heated in collectors only during times when there is available heat
- (c) at the collector, the mixture of water and propylene-glycol is heated and returned to a solar storage tank
- (d) there is an expansion tank with enclosed air chamber to assist water draining

Ans. (c)

98. A PV cell is illuminated with irradiance (E) of 1000 W/m². If the cell is 100 mm × 100 mm in size and produces 3 A at 0.5V at the maximum power point, the conversion efficiency will be

| (a) 15% | (b) 19% |
|---------|---------|
| (c) 23% | (d) 27% |

Ans. (a)

Sol. Conversion efficiency = $\frac{V_m \cdot I_m}{\text{Irradiation} \times \text{area}}$

 $= \frac{3 \times 0.5}{1000 \times 100 \times 100 \times 10^{-6}} = \frac{1.5}{10} \times 100$

= 15%

- 99. In a barrage of 300000 m² area with a tide height of 3, barrage drain time of 10 hr, density of sea water as 1025 kg/m³ and gravitational acceleration as 9.8 m/s², the average power will be
 - (a) 377 kW (b) 381 kW
 - (c) 388 kW (d) 396 kw
- Ans. (a)
- **Sol.** Average power, $P_{avg.} = \frac{W}{t} = \frac{1}{2} \frac{\rho g A R^2}{t}$

 $= \frac{1}{2} \times \frac{1025 \times 9.8 \times 300000 \times 3^2}{10 \times 3600}$

= 377 kW

- **100.** The platinum nano-coating is made on the anode of the fuel cell to
 - (a) Create lighter and more efficient fuel cell membranes
 - (b) Make the fuel effective
 - (c) Create high thermal conductivity in the cell
 - (d) Make the fuel cell non-conductivity in the cell

Ans. (b)

| Sol. Platinum nano-coating make the fuel effect | ive. |
|---|------|
|---|------|

- **101.** In a fuel cell, electric current is produced when
 - (a) Hydrogen and oxygen react with each other and electrons are freed
 - (b) Hydrogen reacts with water and electrons are freed
 - (c) Oxygen reacts with water and electrons are freed
 - (d) Electrons react with molecules of hydrogen and oxygen is freed

Ans. (a)

- **Sol.** They generate electricity from the reaction of hydrogen with oxygen to from a water in a process which is the reverse of electrolysis.
- **102.** Which one of the following is suitable for fuel cell electric vehicle (FCEV)?
 - (a) Direct methanol fuel cell (DMFC)
 - (b) Alkaline fuel cell (AFC)
 - (c) Proton exchange membrane fuel cell (PEMFC)
 - (d) Solid oxide fuel cell (SOFC)
- Ans. (c)
- Sol. PEMFC is used for FCEV fuel cars.
- **103.** A pull of 100 kN acts on a bar as shown in the figure in such a way that it is parallel to the bar axis and is 10 mm away from xx:

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10 mm_x x 80 mm Ρ 50 mm

The maximum bending stress produced in the bar at xx is nearly.

- (b) 18.8 N/mm² (a) 20.5 N/mm²
- (c) 16.3 N/mm² (d) 14.5 N/mm²

Ans. (b)

Sol. Maximum bending stress,

$$\sigma_{max} = \frac{MY}{I} = \frac{100 \times 10^3 \times 40}{\frac{50 \times 80^3}{12}} = 18.8 \text{ N/mm}^2$$

104. The frequency of oscillation is the number of cycles per unit time described by the particle, given by the relation

(a)
$$f = \frac{\omega}{2\pi}$$
 (b) $\frac{1}{f} = \frac{\omega}{2\pi}$
(c) $f' = \frac{2\pi r}{T}$ (d) $f' = \frac{2\pi NT}{T\omega}$

Ans. (a)

105. A particle of mass 1 kg moves in a straight line under the influence of a force which increases linearly with time at the rate of 60N/ s, it being 40 N initially. The position of the particle after a lapse of 5s, if it started from rest at the origin, will be

| (a) 1250 m | (b) 1500 m |
|------------|------------|
| (c) 1750 m | (d) 2000 m |

Ans.

Sol.

(a)

F = kt

F

The motion equation
$$\frac{mdv}{r} = \frac{mdv}{r} = \frac{mdv}{r}$$

dt

The mass of body m = 1 kg

The force varies linearly with time

Where, k is a constant and given as

$$\Rightarrow \frac{dv}{dt} = 60t$$

Integrating it,

$$V = \frac{60-12}{2} + C_1$$

At t = 0, particle starts from origin

Ŀ.

$$C_1 = 0$$

$$V = \frac{ds}{dt} = 30t^2$$

Again integrating,

$$S = \frac{30t^2}{3} + C_2$$
At, $t = 0$, $s = 0$ (origin)
∴ $C = 0$
 $S = 10t^3$
At $t = 5$ sec.
 $S = 10 \times 5^3$
 $= 1250$ m

106. Rails are laid such that there will be no stress in them at 24°C. If the rails are 32 m long with an expansion allowance of 8 mm per rail, coefficient of linear expansion $\alpha = 11 \times 10^{-6/\circ}$ C and E = 205 GPa, the stress in the rails at 80°c will be nearly.

| (a) 68 MPa | (b) 75 MPa |
|------------|------------|
| (c) 83 MPa | (d) 90 Mpa |

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... (i)

k = f/t = 60 t



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Ans. (b)

Sol. Change in length
$$\delta I = \alpha I \Delta T$$

= 11 × 10⁻⁶ × 32 × (80 - 24)
= 19.71 mm
Restrained length $\delta I_{R} = 19.71 - 8 = 1.71$ mm
Stress, $\sigma = \frac{\delta I_{R}}{1} \times E$
= $\frac{11.71}{32 \times 1000} \times 205 \times 10^{9}$
= 75 MPa
107. The loads acting on a 3 mm diameter bar at different points are as shown in the figure:
 $10KN + \frac{B}{2KN} + \frac{C}{3KN} + \frac{D}{3KN}$
If E = 205 GPa, the total elongation of the bar will be nearly.
(a) 29.7 mm
(b) 25.6 mm
(c) 21.5 mm
(d) 17.4 mm
Ans. (a)
Sol.
 $10 \text{ kN} + \frac{B}{10 \text{ kN}} + \frac{C}{8 \text{ kN}} + \frac{C}{5 \text{ kN}} + 5 \text{ kN}$
Total elongation $\Delta I = \frac{1}{AE}(P|I_{1})$
= $\frac{\pi}{4}(0.003)^{2} \times 205 \times 10^{9}$
= 29.7 mm
108. A hollow circular bar used as a beam has its

108. A hollow circular bar used as a beam has its outer diameter thrice the inside diameter. It is subjected to a maximum bending moment of 60 MN m. If the permissible bending stress is

limited to 120 MPa, the inside diameter of the beam will be.

- (a) 49.2 mm
- (b) 53.4 mm (d) 61.8 mm
- (c) 57.6 mm Ans. (575.8 mm)

Sol. Given,

$$D_o = 3D_i \implies \frac{D_o}{D_i} = 3$$

Permissible bending stress,

Γ

$$=\frac{My}{I}$$

$$\sigma_{\rm P} = \frac{M \times \frac{D_{\rm o}}{2}}{\frac{\pi}{64} (D_{\rm o}^4 - D_{\rm i}^4)}$$

$$\sigma_{P} = \frac{32M}{\pi D_{o}^{3} \left[1 - \left(\frac{D_{i}}{D_{o}} \right)^{4} \right]}$$
$$32 \times 60 \times 10^{6}$$

120 × 10⁶=
$$\frac{0.2 \times 00^{-110}}{\pi \times D_0^3 \left[1 - \left(\frac{1}{3}\right)^4 \right]}$$

D₀ = 1.7276 m
∴ D₁ = 0.5758 m

= 575.8 mm

- **109.** In a beam of I-section, which of the following parts will take the maximum shear stress when subjected to traverse loading?
 - 1. Flange
 - 2. Web

Select the correct answer using code given below.

- (a) 1 only (b) 2 only
- (c) Both 1 and 2 (d) Neither 1 or 2



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- Sol. Shear stress distribution in I-section of beam
- **110.** Which of the following statements is/are correct?
 - 1. In uniformly distributed load, the nature of shear force is linear and bending moment is parabolic.
 - 2. In uniformly varying load, the nature of shear force is linear and bending moment is parabolic.
 - 3. Under no loading condition, the nature of shear force is lienar and bending moment is constant.

Select the correct answer using the code given below.

(d) 1 only

- (a) 1 and 2 (b) 1 and 3
- (c) 2 only
- Ans. (d)
- **111.** The cross-section of the beam is as shown in the figure.



If the permissible stress is 150 $\ensuremath{\text{N/mm^2}}\xspace$, the bending moment M will be nearly

(a) 1.21×10^8 N mm

- (b) 1.42×10^8 N mm
- (c) 1.64×10^8 N mm

(d) 1.88 × 10⁸ N mm

Ans. (b)

Sol. Moment of inertia of I-section,

$$I = \left(\frac{200 \times 400^3}{12} - \frac{192 \times 380^3}{12}\right)$$

 $= 191.66 \times 10^{6} \text{ mm}^{4}$

Permissible stress,

$$\sigma_{max} = \frac{MY}{I}$$

$$150 = \frac{M \times 200}{191.66 \times 10^6}$$

... Bending moment,

 $M = 1.42 \times 10^8 Nmm$

- **112.** In a propeller shaft, sometimes apart from bending and twisting, end thrust will also develop stresses which would be
 - (a) Tensile in nature and uniform over the cross-section
 - (b) Compressive in nature and uniform over the cross-section
 - (c) Tensile in nature and non-uniform over the cross-section
 - (d) Compressive in nature and non-uniform over the cross-section

Ans. (b)

113. A spherical shell of 1.2 m internal diameter and 6 mm thickness is filled with water under pressure until volume is increased by 400 × 10^3 mm³. If e = 204 GPa, Poisson's ratio v = 0.3, neglecting radial stresses, the hoop stress developed in the shell will be nearly

| (a) 43 MPa | (b) 38 Mpa |
|------------|------------|
|------------|------------|

(c) 33 Mpa (d) 28 Mpa



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Sol. Since
$$\frac{r}{t} = \frac{600}{6} = 100 > 10$$

so thin pressure vessel case Volumetric strain,

$$\epsilon_{v} = \frac{\Delta V}{V} = \frac{400 \times 10^{3}}{\frac{4}{3}\pi \times 600^{3}} = 4.42097 \times 10^{-4}$$

= 3 × hoop strain (
$$\in_{\theta}$$
)

 \therefore hoop strain, $\in_{\Theta} = 1.4736 \times 10^{-4}$

$$= \frac{\sigma_{\theta}}{\epsilon} (1 - v)$$
$$= \frac{\sigma_{\theta}}{204 \times 10^3} (1 - 0.3)$$

 \therefore hoop stress, $\sigma_{\theta} = 43 \text{ MPa}$

- **114.** The inner diameter of a cylindrical tank for liquefied gas is 250 mm. The gas pressure is limited to 15 MPa. The tank is made of plain carbon steeel with ultimate tensile strength of 340 N/mm², Poisson's ratio of 0.27 and the factor of safety of 5. The thickness of the cylinder wall will be.
 - (a) 60 mm (b) 50 mm
 - (c) 40 mm (d) 30 mm
- Ans. (d)
- **Sol.** Maximum stress = hoop stress in cylinder, Pr

$$\sigma_{h} = \overline{t}$$

$$\frac{\sigma_{u}}{fos} = \frac{Pr}{t}$$

$$\frac{340}{5} = \frac{340}{5} = \frac{15 \times 125}{t}$$

$$t = 27.57 \text{ mm}$$

- **115.** The structure of sodium chloride is considered as
 - (a) A body-centred crystal

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- (b) A simple cubic crystal
 - (c) Two interpenetrating FCC sub lattices of Cl^ ions and Na^ ions
- (d) A cubic crystal with Na⁺ and Cl⁻ alternatively at the cubic corners

Ans. (c)

Sol. The structure of NaCl is considered as two interpenetrating FCC subtitute of Cl ions and Na⁺ ions.

116. Hardenability of steel is assessed by

- (a) Charpy impact test
- (b) Rockwell hardnes test
- (c) Jominy end-quench test
- (d) Open hole test

Ans. (c)

- **117.** A metal has lattice parameter of 2.9 Å, density of of 7.87 g/cc, atomic weight of 55.85, and Avogadro's number is 6.0238 \times 10²³. The number of atoms per unit cell will be nearly.
 - (a) 1 (b) 2
 - (c) 8 (d) 16

Ans. (b)

Sol. Density, $\rho = \frac{n.A}{V_c \cdot N_A}$

n = no. of atoms (is to be determined)

A = Atomic weight = 55.85

 V_c = volume of unit cell

$$V_c = a^3 = (2.9 \times 10^{-10})^3 m^3$$

 N_A = Avogado's Number

$$\rho$$
 = 7.87 gm/cc = 7.87 × 10⁶ gm/m³

$$\Rightarrow 7.87 \times 10^{6} = \frac{n \times 55.85}{(2.9 \times 10^{-10})^{3} \times 6.023 \times 10^{23}}$$
$$\Rightarrow \boxed{n = 2.06 \approx 2}$$



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$$= \frac{0.2}{1.2 \times 10^{-3}} = \frac{1000}{6} \sec^{-1}$$
So. $\frac{15000}{128} = \mu \times \frac{1000}{6}$
 $\Rightarrow \quad \mu = \frac{15 \times 6}{128} = \frac{90}{123}$
 $\boxed{\mu = 0.70 \frac{N-S}{m^2}}$
123. A spherical ballon of 1.5 m diameter is
completely immersed in water and chained to
the bottom. If the chain has a tension of 10
NN, the weight of the balloon will be nearly
(a) 9.11 kN (b) 8.22 kN
(c) 6.44 kN (d) 7.33 kN
Ans. (d)
Sol.
Ballon $\int F(Buoyanoy force)$
 $\int F(Buoyanoy force)$
 $\int F(Buoyanoy force)$
 $\int Weight, W$
 $Tension, T$
So, $F = W + T$
 $\Rightarrow W = F - T$
Weight, $W = p.gV - T$
 $[:: p = Density of water]$
 $[:: p = Density of water]$
Ans. (a)
 $I = 1000 \times 9.81 \times \frac{\pi(1.5)^2}{6} - 10$
 $= 17.33 - 10$
 $W = 7.33 kN$
124. A nozzle at the end of an 80 mm hosepipe
produces a jet 40 mm in diameter. When it is
discharging the water 1200 vp, the force on
the joint at the base of the nozzle will be
(a) 180 N (b) 200 N
(b) 200 N
(c) 220 N (d) 240 N
Ans. (d)
Sol.
 $I = pQ(V_2 - V_1) \dots (i)$
 $\therefore V_1 = \frac{0}{A_1} = \frac{1.2 \times 4}{60 \times \pi \times (0.08)} = 3.98 m / sec$
 $V_2 = 4V_1 = 15.9155 m/s$
 $\therefore F = pQ(V_2 \cdot V_2) = \frac{100 \times 1.2}{60} (15.9155 - 398)$
 $= 238.71 N$
125. A vertical water pipe 1.5 m long, taper from
75 mm diameter at the bottom to 150 mm
diameter at the bottom to 150 mm
form diameter at the bottom to 150 mm
diameter athe bottom to 150 mm
diameter at the bottom

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126.



Applying Bernoulli's equation between (1) and (2)

- $\begin{aligned} \frac{P_1}{\rho g} + \frac{v_1^2}{2g} + z_1 &= \frac{P_2}{\rho g} + \frac{v_2^2}{2g} \\ \therefore \quad Q = v_1 A_1 = v_2 A_2 \\ \Rightarrow \quad \frac{P_1}{\rho g} + \frac{Q^2 \times 16}{2 \times g \cdot \pi^2 \cdot d_1^4} + z_1 &= \frac{P_2}{\rho g} + \frac{Q^2 \times 16}{2 \cdot g \cdot \pi^2 \cdot d_2^4} \\ \Rightarrow \quad \frac{P_1}{\rho g} &= \frac{150 \times 10^3}{10^3 \times 9.81} + \frac{(0.05)^2 \times 16}{2 \times \pi^2 \times 9.81 \times (0.075)^4} \\ &- \frac{(0.05)^2 \times 16}{2 \times \pi^2 \times 9.81 \times (0.15)^4} 1.5 \\ \frac{P_1}{\rho g} &= 19.91 \\ \Rightarrow \quad P_1 &= 1000 \times 9.81 \times 19.91 \\ \text{Pressure at the top of the pipe,} \\ \hline P_1 &= 195.327 \text{ kN/m}^2 \\ \end{bmatrix} \\ \text{The stream function for a flow field is } \psi = 3x^2 \text{ y} + (2 + t)y^2. \text{ The velocity at a point P for position vector } r = i + 2j \text{ time } t = 2 \text{ will be} \end{aligned}$
- (a) 19i 12j (b) 21 i 12 j
- (c) 19i + 22j (d) 21 i + 22j

Ans. (a)

Sol.
$$\Psi = 3xzy + (2 + t)y^2$$

$$u = \frac{\partial \psi}{\partial y} = 3x^2 + 2(2 + t)y = 3 + 8 \times 2 = 19$$

$$y = -\frac{\partial \psi}{\partial x} = 6xy + 0 = -6 \times 1 \times 2 = -12$$

$$\overline{y} = u\hat{i} + v\hat{i} = 19\hat{i} - 12\hat{i}$$

- **127.** In a laminr flow through pipe, the point of maximum instability exists at a distance of y fro the wall which is
 - (a) $\frac{3}{2}$ of pipe radius R (b) $\frac{2}{3}$ of pipe radius R
 - (c) $\frac{1}{2}$ of pipe radius R
 - (d) $\frac{1}{3}$ of pipe radius R

Ans. (b)

$$u = V_{max} \left(1 - \frac{r^2}{R^2} \right)$$

 $\therefore \qquad \frac{du}{dr} = \frac{-du}{dy}$

$$\therefore \quad \frac{du}{dy} = \frac{+2V_{max}r}{R^2} = \frac{2V_{max} \cdot r}{R^2} = \frac{2V_{max}(R-y)}{R^2}$$
$$\therefore \quad X = 2y^2 \frac{\rho V_{max}r}{R^2} = (R-y) \qquad \dots (ii)$$

Differentiaty and equal to zero

$$\frac{dx}{dy} = \frac{2fV_{max}}{\mu R^2} \frac{d}{dy} (Ry^2 - y^3) = 0$$

. 2Ry - 3y² = 0
. y(2R - 3y) = 0
. y = 0

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$$y = \frac{2R}{3}$$
128.
$$Q = \frac{\partial u'}{\partial x} = \frac{-\partial v'}{\partial y} \text{ for a turbulent flow signifies}$$
(a) Conservation of bulk momentum transport
(b) Increase in u' in x-direction followed vby
increase in v' in negative y-direction
(c) Turbulence is anisotropic
(d) Turbulence is anisotropic
(d) Turbulence is isotropic
Ans. (b)
129. A flow field satisfying $\Delta \cdot \bar{V} = 0$ as the
continuity equation represents always
(a) A steady compressible flow
(b) An incompressible flow
(c) an unsteady and incompressible flow
(d) an unsteady and compressible flow
Ans. (b)
Sol. Equation of continuity,

$$\rho(\nabla \cdot \bar{v}) + \frac{\Delta p}{\Delta t} = 0$$
For incompressible flow,

$$\nabla \cdot \bar{v} = 0$$

$$\nabla \cdot \bar{v} = 0$$

$$\nabla \cdot \bar{v} = 0$$

$$\frac{\nabla \cdot \bar{v}}{\partial t} = 0$$

$$\nabla \cdot \bar{v} = 0$$

$$\frac{\nabla \cdot \bar{v}}{\partial t} = 0$$

130. An oil of viscosity 8 poise flows between two parallel fixed plates, which are kept at a distance of 30 mm apart. If the drop of pressure for a length of 1m is $0.3 \times 10^4 \text{ N/m}^2$ and width of the plates is 500 mm, the rate of oil flow between the plates will be

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(c)
$$6.6 \times 10^{-3} \text{ m}^{3/\text{s}}$$

Ans. (a)

Pressure head loss, Sol.

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of

ble

$$= \omega \left(\frac{\pi D^2}{4} V \right) \left(H - \frac{f V^2}{2g D} \right) = \omega \frac{\pi}{4} D^2 \left(H V - \frac{f I V^3}{2g D} \right)$$

For maximum power,

$$\frac{dP}{dV} = \omega \left(\frac{\pi}{4}D^2\right) \left(H - \frac{3fIV^2}{2gD}\right) = 0$$

$$\Rightarrow H = 3h_f$$

i.e. power transmitted through a pipe is

maximum if head loss due to friction is $\frac{1}{3}$ of total head loss.

: Efficiency,

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$$\eta_{max} = \frac{H - h_f}{H} = \frac{3h_f - h_f}{3h_f} = \frac{2}{3} = 66.7\%$$

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- **132.** A pipe having a length 200 m and 200 mm diameter with friction factor 0.015, is to be replaced by a 400 mm diameter pipe of friction factor 0.012 to convey the same quantity of flow. The equivalent length of the new pipe for the same head loss will
 - (a) 8300 m (b) 8240 m
 - (c) 8110 m (d) 8000 m
- Ans. (d)
- **Sol.** $h_f = \frac{f \ell Q^2}{12.1 d^5}$

For same discharge and head loss,

$$\frac{f_1 \ell_1}{d_1^5} = \frac{f_2 \ell_2}{d_2^5}$$
$$\frac{0.015 \times 200}{200^5} = \frac{0.012 \times \ell_2}{400^5}$$
$$\ell_2 = 8000 \text{ m}$$

- **133.** Certain quantities cannot be located on the graph by a point but are given by a point but are given by the area under the curve corresponding to the process. These quantities in concepts of thermodynamics are called as
 - (a) cyclic functions (b) point functions
 - (c) path functions (d) real functions
- Ans. (c)
- **Sol.** Path functions like heat transfer and work transfer cant be represented by points in the graph, but can be given by the area under the curve.

Ex: heat transfer will be area under curve in T-s diagram work transfer will be area under curve in P-V diagram.

134. When 25 kg of water at 95°C is mixed with 35 kg of water at 35°C, the pressure being taken

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as constant at surrounding temperature of 15°C and C_p of water is 4.2 kJ/kg K, the decrease in available energy due to mixing will be nearly

(a) 270.5 kJ (b) 277.6 kJ

(c) 281.8 kJ (d) 288.7 kJ

Ans. (c)

Sol. After mixing, if t°C in the final temepratue, then $25 \times 4.2 \times (45 - t) = 35 \times 4.2 \times (t - 35)$

$$t = \frac{25 \times 95 + 35 \times 35}{25 + 35} = 60^{\circ}C$$

Available energy =
$$mCp\left[(T - T_o) - T_o ln \frac{T}{T_o}\right]$$

· Available energy of 25 kg water at 95°C

$$A_{25} = 25 \times 4.2 \times \left[(368 - 288) - 288 \ln \frac{368}{288} \right]$$

= 987.49 kJ

Available energy of 35 kg water at 35°C

$$A_{35} = 35 \times 4.2 \times \left[(308 - 288) - 288 \ln \frac{308}{288} \right]$$

Final available of 60 kg water at 60°C,

$$A_{60} = 60 \times 4.2 \times \left[(333 - 288) - 288 \ln \frac{333}{288} \right]$$

= 803.27 kJ

 \therefore Decrease in available energy due to mixing

$$A_{25} + A_{35} - A_{60} = (987.49 + 97.59 - 803.27)$$

= 281.8 kJ

135. A frictionless pistion cylinder device contains 5 kg of steam at 400 kPa and 200°C. The heat is now transferred to the stam until the temperature reaches 250°C. If the piston is not attached to a shaft, its mass is constant and by taking the values of specific volume v_1



Ans. (b) as 0.53434 m³/kg and v_2 as 0.529520 m³/kg the work done by the steam during this Mass fraction of O₂ = $\frac{m_{O_2}}{m_{O_2} + m_{N_2} + m_{CH_2}}$ process is Sol. (b) 137.5 kJ (a) 121.7 kJ $=\frac{3}{3+5+12}=\frac{3}{20}=0.15$ (c) 153.3 kJ (d) 189.1 kJ Ans. (a) Mole fraction of $O_2 = \frac{n_{O_2}}{n_{O_2} + n_{N_2} + n_{CH}}$ Sol. Since the weight of the piston and the atmosphere presssure are constant, so assuming it as a constant pressure process, Work done, $W = P(V_2 - V_1)$ $= \frac{\frac{32}{32}}{\frac{3}{32} + \frac{5}{28} + \frac{12}{6}} = 0.092$ $= P \times m (v_2 - v_1)$ $= 400 \times 10^3 \times 5 \times (0.59520 - 0.53434)$ = 121.72 kJ 138. An insulated pipe of 50 mm outside diameter with $\varepsilon = 0.8$ is laid in a room at 30°C. If the A diesel engine has a compression ratio of 14 136. surface temperature is 250°C and the and cutoff takes place at 6% of the stroke. convective heat transfer coefficient is 10W/ The air standard efficiency will be m²K, the total heat loss per unit length of the (a) 74.5% (b) 60.5% pipe will be (d) 44.5% (c) 52.5% (b) 818.8 w/m (a) 896.6 W/m Ans. (b) (c) 786.4W/m (d) 742.2 W/m $(V_3 - V_2 = 0.06(V_1 - V_2))$ Sol. Ans. (b) Sol. $\left(\frac{V_3}{V_2} - 1\right) = 0.06 \left(\frac{V_1}{V_2} - 1\right)$ T_s = 250°C $h = 10W/m^{2}K$ \Rightarrow (r_c - 1) = 0.06(r - 1) ∈ = 0.8 \Rightarrow (r_c - 1) = 0.06(14 - 1) 50 mm \Rightarrow $r_c = 1.78$ Room at 30°C Total heal loss per unit length of the pipe $\eta = 1 - \frac{1}{(r)^{\gamma-1}} \left[\frac{r_{c}^{\gamma} - 1}{\gamma(r_{c} - 1)} \right]$ $= Q_{conv.} + Q_{rad}$ = $h_{conv} \cdot A_s (T_s - T_{room}) + \in \sigma A_s (T_s^4 - T_{room}^4)$ = 60.43% $= A_{s} \Big[h_{conv} + \in \sigma(T_{s} + T_{room}) \big(T_{s}^{2} + T_{room}^{2} \big) \Big] \big(T_{s} - T_{room} \big)$ **137.** A gas mixture consists of 3 kg of O₂, 5kg of N₂ and 12 kg of CH₄. The mass fraction and mole fraction and mole fraction of O₂ are $=2\pi \times 0.025 [10 + 0.8 \times 5.67 \times 10^{-8} (523 + 303)]$ (a) 0.25 and 0.125 (b) 0.15 and 0.092 $(523^2 + 303^2)$ (523 - 303) = 818.6 (c) 0.25 and 0.092 (d) 0.15 and 0.125

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- 139. A wire of 8 mm diameter at a temperature of 60°C is to be insulated by a material having k = 0.174 W/mK. The heat transfer coefficient on the outside $h_a = 8W/m^2K$ and ambient temeprature $T_a = 25^{\circ}C$. The maximum thickness of insulation for maximum heat loss will be
 - (a) 15.25 mm (b) 16.50 mm
 - (c) 17.75 mm (d) 18.25 mm
- Ans. (c)
- Given maximum heat loss, critical radius of Sol. insulation.

$$r_{c} = \frac{k}{h} = \frac{0.174}{8} = 0.02175m = 21.75mm$$

: Maximum thickness of insulation of maximum heat loss

- In liquid metals, thermal boundary layer 140. develops much faster than velocity boudnary layer due to
 - (a) Lower value of Nusselt number
 - (b) Higher value of Prandtl number
 - (c) Lower value of Prandtl number
 - (d) Higher value of Nusselt number

Ans. (c)

Prandtl number (P_r) = $\frac{\delta}{\delta_{th}}$ Sol.

For liquid metals, Prandtl number $(P_r) < 1$

- The temperature of a body of area 0.1 m² is 141. 900 K. The wavelength for maximum monochromatic emissive power will be nearly
 - (a) 2.3µm (b) 3.2µm
 - (d) 5.0µm (c) 4.1µm
- Ans. (b)
- Sol. From Wien's displacement law

 $\lambda_{max} T = 2898$

 $\lambda_{max} \times 900 = 2898$ λ_{max} = 3.2µm

142. Consider the following statements:

> For the laminar condensation on a verticla plate, the Nussel theory says that

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- 1. Inertia force in the film is negligible compared to viscosity and weight
- 2. Heat flow is mainly by conduction through the liquid film, convection inliquid film as well as in vapour is neglected
- 3. Velocity of vapour is very high

Which of the above statements are correct?

- (a) 1, 2 and 3 (b) 1 and 2 only
- (d) 2 and 3 only (c) 1 and 3 only

Ans. (b)

- Sol. The velocity of the vapor is low (or zero) so that it exerts no drag on the condensate (no viscous shear on the liquid -vapor interface).
- 143. In transiton boiling heat flux decreases due to which of the following?
 - 1. Low value of film heat transfer coefficient at the surface during 100°C to 120°C surface temperature
 - 2. Major portion of heater surface is covered by vapour film which has smaller thermal conductivity as compared to liquid
 - 3. Nucleate boiling occurs very fast

Select the correct answer using the code given below.

(b) 2 only (a) 1 only

(d) 1, 2 and 3 (c) 3 only

- Ans. (b)
- Sol. In transition boiling heat flux decreases because a large fraction of the heater surface is covered by a vapor film, which acts as an insulation due to the low thermal conductivity of the vapor relative to that of the liquid.







Expected number of fires in one minute

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$$=\frac{506}{2}\times 6=1518$$

- \therefore Number of misfires/min = 1518 1500 = 18
- ... Average number of misfires per min per cylinder,

$$=\frac{18}{6}=3$$

- **148.** Which one of the following compressors will be used in vapour compression refrigerator for plants up to 100 tonnes capacity?
 - (a) Reciprocating compressor
 - (b) Rotary compressor
 - (c) Centrifugal compressor
 - (d) Double-acting compressor

Ans. (a)

- **Sol.** Reciprocating compressors are used in plants upto 100 tonnes capacity. For plants of higher capacities, centrifugal compressors are employed.
- 149. A cold storage is to be maintained at -5°C while the surroundings are at 35°C. The heat leakage from the surroundings into the cold storage is estimated to be 29 kW. The actual

COP of the refrigeration plant used is $\frac{1}{3}$ rd

that of an ideal plant working between the same temperatures. The power required to drive the plant will be

(d) 16 kW

- (a) 13 kW (b) 14 kW
- (c) 15 kW

Ans. (a) Sol.



$$T_{1} = 35 + 273 = 308 \text{ K}$$

$$T_{2} = 273 - 5 = 268 \text{ K}$$
Carnot COP = $\frac{T_{2}}{T_{1} - T_{2}}$

$$= \frac{268}{308 - 268} = \frac{268}{40} = 6.7$$
∴ Actual COP = $\frac{1}{3} \times \text{carnot COP} = \frac{6.7}{4}$

$$\therefore \text{ Actual COP} = \frac{Q_{2}}{2}$$

 $Q_{2} = 29 \text{ kW}$

$$\int \frac{29 \times 3}{29 \times 3}$$

$$\Rightarrow W = \frac{Q_2}{\text{Actual COP}} = \frac{29 \times 3}{6.7} = 12.985 \text{ kW}$$
$$\approx 13 \text{ kW}$$

150. Consider the following statements:

An expansion device in a refrigeration system

- (1) reduces the pressure from the condenser to the evaporator
- (2) regulates the flow of the refrigerant to the evaporator depending on the load
- (3) is essentially a restriction offering resistance to flow

Which of the above statements are correct?

- (a) 1 and 2 only (b) 1 and 3 only
- (c) 2 and 3 only (d) 1, 2 and 3

Ans. (d)

Sol. An expansion device in a refrigeration system expands the liquid refrigerant from the condenser pressure to the evaporator pressure. The expansion device also controls the supply of the liquid to the evaporator at the rate at which it is evaporated. The expansion device is essentially a restriction.