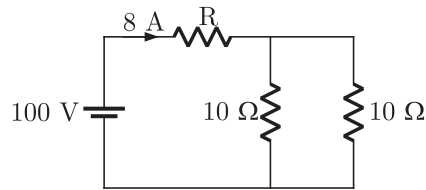


### Q.1 - 30 Carry One Mark Each

**Q.1** In the figure given below the value of  $R$  is

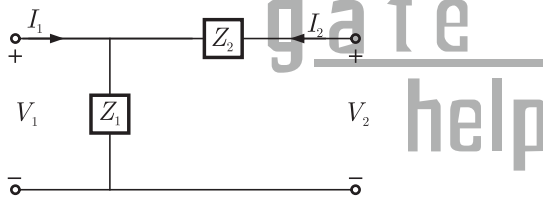


- (A) 2.5  $\Omega$  (B) 5.0  $\Omega$   
 (C) 7.5  $\Omega$  (D) 10.0  $\Omega$

**Q.2** The RMS value of the voltage  $u(t) = 3 + 4 \cos(3t)$  is

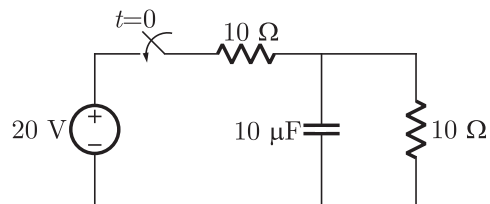
- (A)  $\sqrt{17}$  V (B) 5 V  
 (C) 7 V (D)  $(3 + 2\sqrt{2})$  V

**Q.3** For the two port network shown in the figure the  $Z$ -matrix is given by



- (A)  $\begin{bmatrix} Z_1 & Z_1 + Z_2 \\ Z_1 + Z_2 & Z_2 \end{bmatrix}$  (B)  $\begin{bmatrix} Z_1 & Z_1 \\ Z_1 + Z_2 & Z_2 \end{bmatrix}$   
 (C)  $\begin{bmatrix} Z_1 & Z_2 \\ Z_2 & Z_1 + Z_2 \end{bmatrix}$  (D)  $\begin{bmatrix} Z_1 & Z_1 \\ Z_1 & Z_1 + Z_2 \end{bmatrix}$

**Q.4** In the figure given, for the initial capacitor voltage is zero. The switch is closed at  $t = 0$ . The final steady-state voltage across the capacitor is



- (A) 20 V (B) 10 V  
(C) 5 V (D) 0 V

**Q.5** If  $\vec{E}$  is the electric intensity,  $\nabla(\nabla \times \vec{E})$  is equal to

- (A)  $\vec{E}$  (B)  $|\vec{E}|$   
(C) null vector (D) Zero

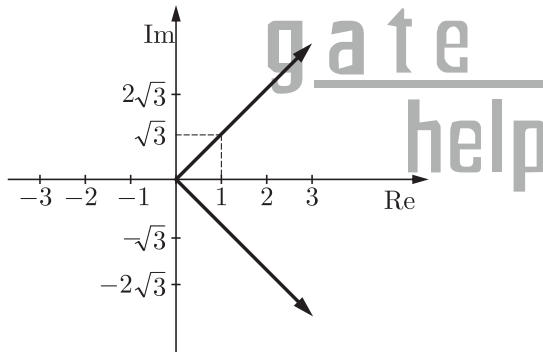
**Q.6** A system with zero initial conditions has the closed loop transfer function.

$$T(s) = \frac{s^2 + 4}{(s + 1)(s + 4)}$$

The system output is zero at the frequency

- (A) 0.5 rad/sec (B) 1 rad/sec  
(C) 2 rad/sec (D) 4 rad/sec

**Q.7** Figure shows the root locus plot (location of poles not given) of a third order system whose open loop transfer function is



- (A)  $\frac{K}{s^3}$  (B)  $\frac{K}{s^2(s+1)}$   
(C)  $\frac{K}{s(s^2+1)}$  (D)  $\frac{K}{s(s^2-1)}$

**Q.8** The gain margin of a unity feed back control system with the open loop transfer function

$$G(s) = \frac{(s+1)}{s^2} \text{ is}$$

- (A) 0 (B)  $\frac{1}{\sqrt{2}}$   
(C)  $\sqrt{2}$  (D)  $\infty$

**Q.9** In the matrix equation  $P\mathbf{x} = \mathbf{q}$ , which of the following is a necessary condition for the existence of at least one solution for the unknown vector  $\mathbf{x}$

- (A) Augmented matrix  $[P\mathbf{q}]$  must have the same rank as matrix  $P$
- (B) Vector  $\mathbf{q}$  must have only non-zero elements
- (C) Matrix  $P$  must be singular
- (D) Matrix  $P$  must be square

**Q.10** If  $P$  and  $Q$  are two random events, then the following is TRUE

- (A) Independence of  $P$  and  $Q$  implies that probability  $(P \cap Q) = 0$
- (B) Probability  $(P \cup Q) \geq$  Probability  $(P) +$  Probability  $(Q)$
- (C) If  $P$  and  $Q$  are mutually exclusive, then they must be independent
- (D) Probability  $(P \cap Q) \leq$  Probability  $(P)$

**Q.11** If  $S = \int_1^\infty x^{-3} dx$ , then  $S$  has the value

- (A)  $-\frac{1}{3}$
- (C)  $\frac{1}{2}$

(B)  $\frac{1}{4}$

(D) 1

**Q.12** The solution of the first order differential equation  $x'(t) = -3x(t)$ ,  $x(0) = x_0$  is

- (A)  $x(t) = x_0 e^{-3t}$
- (B)  $x(t) = x_0 e^{-3}$
- (C)  $x(t) = x_0 e^{-1/3}$
- (D)  $x(t) = x_0 e^{-1}$

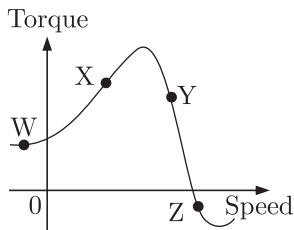
**Q.13** The equivalent circuit of a transformer has leakage reactances  $X_1, X_2$  and magnetizing reactance  $X_M$ . Their magnitudes satisfy

- (A)  $X_1 \gg X_2 \gg X_M$
- (B)  $X_1 \ll X_2 \ll X_M$
- (C)  $X_1 \approx X_2 \gg X_M$
- (D)  $X_1 \approx X_2 \ll X_M$

**Q.14** Which three-phase connection can be used in a transformer to introduce a phase difference of  $30^\circ$  between its output and corresponding input line voltages

- (A) Star-Star (B) Star-Delta  
(C) Delta-Delta (D) Delta-Zigzag

**Q.15** On the torque/speed curve of the induction motor shown in the figure four points of operation are marked as W, X, Y and Z. Which one of them represents the operation at a slip greater than 1 ?



- (A) W (B) X  
(C) Y (D) Z

**Q.16** For an induction motor, operation at a slip  $s$ , the ration of gross power output to air gap power is equal to

- (A)  $(1 - s)^2$  (B)  $(1 - s)$   
(C)  $\sqrt{(1 - s)}$  (D)  $(1 - \sqrt{s})$

**Q.17** The p.u. parameter for a 500 MVA machine on its own base are:

inertia,  $M = 20$  p.u. ; reactance,  $X = 2$  p.u.

The p.u. values of inertia and reactance on 100 MVA common base, respectively, are

- (A) 4, 0.4 (B) 100, 10  
(C) 4, 10 (D) 100, 0.4

**Q.18** An 800 kV transmission line has a maximum power transfer capacity of  $P$ . If it is operated at 400 kV with the series reactance unchanged, the new maximum power transfer capacity is approximately

- (A)  $P$  (B)  $2P$   
(C)  $P/2$  (D)  $P/4$

**Q.19** The insulation strength of an EHV transmission line is mainly governed by

- (A) load power factor (B) switching over-voltages

- (C) harmonics (D) corona

**Q.20** High Voltage DC (HVDC) transmission is mainly used for

- (A) bulk power transmission over very long distances  
 (C) inter-connecting two systems with same nominal frequency  
 (C) eliminating reactive power requirement in the operation  
 (D) minimizing harmonics at the converter stations

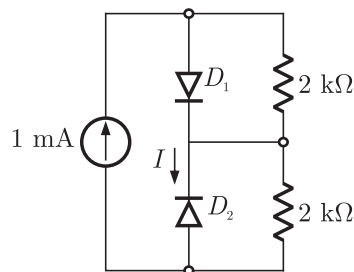
**Q.21** The Q-meter works on the principle of

- (A) mutual inductance (B) self inductance  
 (C) series resonance (D) parallel resonance

**Q.22** A PMMC voltmeter is connected across a series combination of DC voltage source  $V_1 = 2$  V and AC voltage source  $V_2(t) = 3\sin(4t)$  V. The meter reads

- (A) 2 V (B) 5 V  
 (C)  $(2 + \sqrt{3}/2)$  V (D)  $(\sqrt{17}/2)$  V

**Q.23** Assume that  $D_1$  and  $D_2$  in figure are ideal diodes. The value of current is

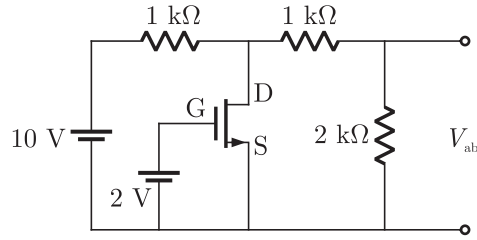


- (A) 0 mA (B) 0.5 mA  
 (C) 1 mA (D) 2 mA

**Q.24** The 8085 assembly language instruction that stores the content of H and L register into the memory locations  $2050_H$  and  $2051_H$ , respectively is

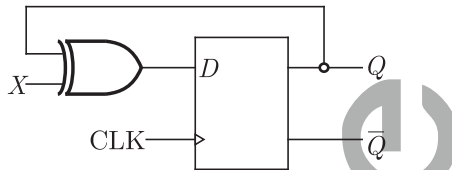
- (A) SPHL  $2050_H$  (B) SPHL  $2051_H$   
 (C) SHLD  $2050_H$  (D) STAX  $2050_H$

**Q.25** Assume that the N-channel MOSFET shown in the figure is ideal, and that its threshold voltage is  $+1.0$  V the voltage  $V_{ab}$  between nodes  $a$  and  $b$  is



- (A) 5 V (B) 2 V  
(C) 1 V (D) 0 V

**Q.26** The digital circuit shown in the figure works as



- (A) JK flip-flop (B) Clocked RS flip-flop  
(C) T flip-flop (D) Ring counter

**Q.27** A digital-to-analog converter with a full-scale output voltage of 3.5 V has a resolution close to 14 mV. Its bit size is

- (A) 4 (B) 8  
(C) 16 (D) 32

**Q.28** The conduction loss versus device current characteristic of a power MOSFET is best approximated by

- (A) a parabola  
(B) a straight line  
(C) a rectangular hyperbola  
(D) an exponentially decaying function

**Q.29** A three-phase diode bridge rectifier is fed from a 400 V RMS,

50 Hz, three-phase AC source. If the load is purely resistive, then peak instantaneous output voltage is equal to

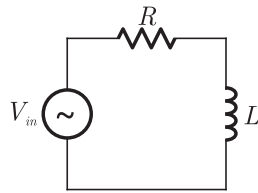
- (A) 400 V (B)  $400\sqrt{2}$  V  
 (C)  $400\sqrt{\frac{2}{3}}$  V (D)  $\frac{400}{\sqrt{3}}$  V

**Q.30** The output voltage waveform of a three-phase square-wave inverter contains

- (A) only even harmonics (B) both odd and even harmonic  
 (C) only odd harmonics (D) only triple harmonics

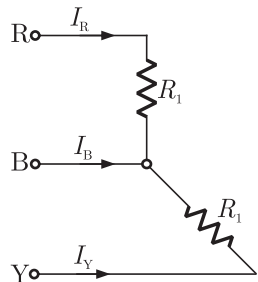
**Q.31 - 80 Carry Two Marks Each**

**Q.31** The RL circuit of the figure is fed from a constant magnitude, variable frequency sinusoidal voltage source  $V_{in}$ . At 100 Hz, the  $R$  and  $L$  elements each have a voltage drop  $\mu_{RMS}$ . If the frequency of the source is changed to 50 Hz, then new voltage drop across  $R$  is



- (A)  $\sqrt{\frac{5}{8}} u_{RMS}$  (B)  $\sqrt{\frac{2}{3}} u_{RMS}$   
 (C)  $\sqrt{\frac{8}{5}} u_{RMS}$  (D)  $\sqrt{\frac{3}{2}} u_{RMS}$

**Q.32** For the three-phase circuit shown in the figure the ratio of the currents  $I_R: I_Y: I_B$  is given by

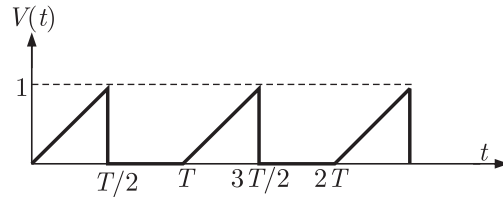


- (A)  $1:1:\sqrt{3}$  (B)  $1:1:2$

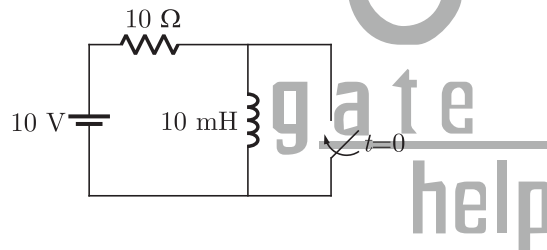
(C) 1:1:0

(D) 1:1: $\sqrt{3/2}$ 

**Q.33** For the triangular wave from shown in the figure, the RMS value of the voltage is equal to

(A)  $\sqrt{\frac{1}{6}}$ (B)  $\sqrt{\frac{1}{3}}$ (C)  $\frac{1}{3}$ (D)  $\sqrt{\frac{2}{3}}$ 

**Q.34** The circuit shown in the figure is in steady state, when the switch is closed at  $t = 0$ . Assuming that the inductance is ideal, the current through the inductor at  $t = 0^+$  equals



(A) 0 A

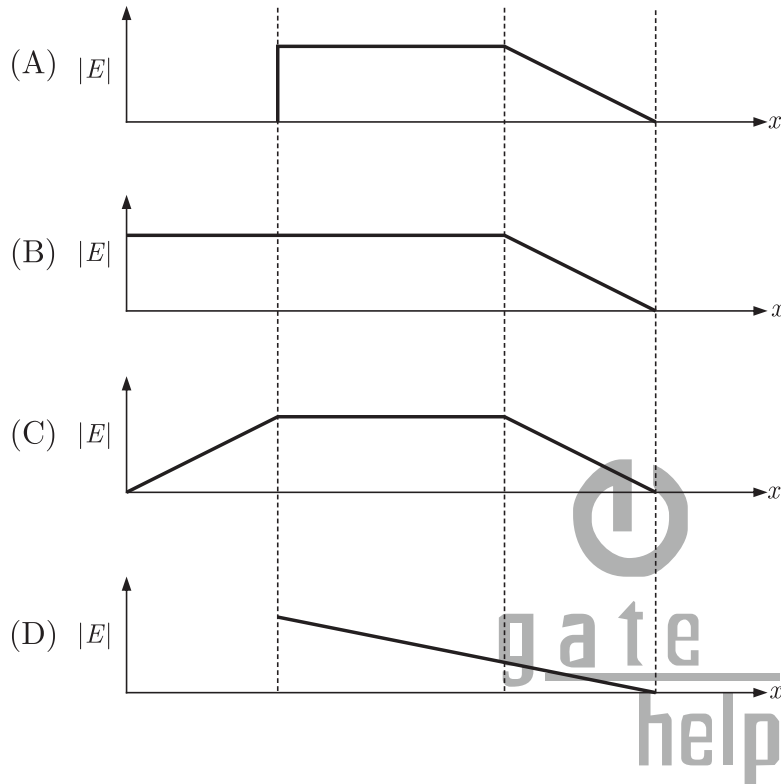
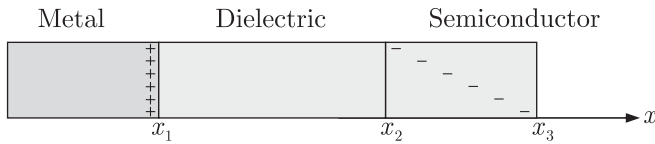
(B) 0.5 A

(C) 1 A

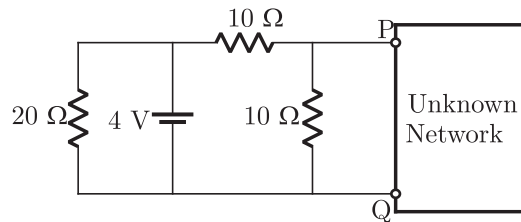
(D) 2 A

**Q.35** The charge distribution in a metal-dielectric-semiconductor specimen is shown in the figure. The negative charge density decreases linearly in the semiconductor as shown. The electric field distribution is as shown in





**Q.36** In the given figure, the Thevenin's equivalent pair (voltage, impedance), as seen at the terminals P-Q, is given by



- (A) (2 V, 5  $\Omega$ )
- (B) (2 V, 7.5  $\Omega$ )
- (C) (4 V, 5  $\Omega$ )
- (D) (4 V, 7.5  $\Omega$ )

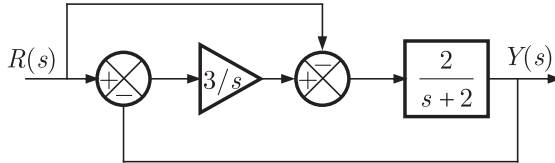
**Q.37** A unity feedback system, having an open loop gain

$$G(s)H(s) = \frac{K(1-s)}{(1+s)}$$

becomes stable when

- (A)  $|K| > 1$  (B)  $K > 1$   
 (C)  $|K| < 1$  (D)  $K < -1$

**Q.38** When subject to a unit step input, the closed loop control system shown in the figure will have a steady state error of

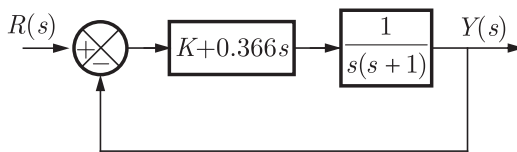


- (A)  $-1.0$  (B)  $-0.5$   
 (C)  $0$  (D)  $0.5$

**Q.39** In the  $G(s)H(s)$ -plane, the Nyquist plot of the loop transfer function  $G(s)H(s) = \frac{\pi e^{-0.25s}}{s}$  passes through the negative real axis at the point

- (A)  $(-0.25, j0)$  (B)  $(-0.5, j0)$   
 (C)  $0$  (D)  $0.5$

**Q.40** If the compensated system shown in the figure has a phase margin of  $60^\circ$  at the crossover frequency of 1 rad/sec, then value of the gain  $K$  is



- (A)  $0.366$  (B)  $0.732$   
 (C)  $1.366$  (D)  $2.738$

**Q.41** For the matrix  $p = \begin{bmatrix} 3 & -2 & 2 \\ 0 & -2 & 1 \\ 0 & 0 & 1 \end{bmatrix}$ , one of the eigen values is equal to  $-2$

Which of the following is an eigen vector ?

- (A)  $\begin{bmatrix} 3 \\ -2 \\ 1 \end{bmatrix}$  (B)  $\begin{bmatrix} -3 \\ 2 \\ -1 \end{bmatrix}$

$$(C) \begin{bmatrix} 1 \\ -2 \\ 3 \end{bmatrix}$$

$$(D) \begin{bmatrix} 2 \\ 5 \\ 0 \end{bmatrix}$$

**Q.42** If  $R = \begin{bmatrix} 1 & 0 & -1 \\ 2 & 1 & -1 \\ 2 & 3 & 2 \end{bmatrix}$ , then top row of  $R^{-1}$  is

$$(A) [5 \ 6 \ 4]$$

$$(B) [5 \ -3 \ 1]$$

$$(C) [2 \ 0 \ -1]$$

$$(D) [2 \ -1 \ 1/2]$$

**Q.43** A fair coin is tossed three times in succession. If the first toss produces a head, then the probability of getting exactly two heads in three tosses is

$$(A) \frac{1}{8}$$

$$(B) \frac{1}{2}$$

$$(C) \frac{3}{8}$$

$$(D) \frac{3}{4}$$

**Q.44** For the function  $f(x) = x^2 e^{-x}$ , the maximum occurs when  $x$  is equal to

$$(A) 2$$

$$(B) 1$$

$$(C) 0$$

$$(D) -1$$

**Q.45** For the scalar field  $u = \frac{x^2}{2} + \frac{y^2}{3}$ , magnitude of the gradient at the point (1, 3) is

$$(A) \sqrt{\frac{13}{9}}$$

$$(B) \sqrt{\frac{9}{2}}$$

$$(C) \sqrt{5}$$

$$(D) \frac{9}{2}$$

**Q.46** For the equation  $x''(t) + 3x'(t) + 2x(t) = 5$ , the solution  $x(t)$  approaches which of the following values as  $t \rightarrow \infty$  ?

$$(A) 0$$

$$(B) \frac{5}{2}$$

$$(C) 5$$

$$(D) 10$$

**Q.47** The Laplace transform of a function  $f(t)$  is  $F(s) = \frac{5s^2 + 23s + 6}{s(s^2 + 2s + 2)}$  as  $t \rightarrow \infty$ ,  $f(t)$  approaches

- (A) 3 (B) 5  
 (C)  $\frac{17}{2}$  (D)  $\infty$

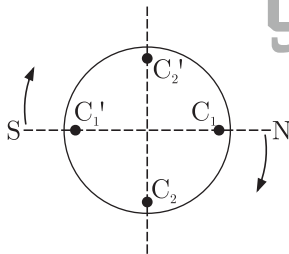
**Q.48** The Fourier series for the function  $f(x) = \sin^2 x$  is

- (A)  $\sin x + \sin 2x$  (B)  $1 - \cos 2x$   
 (C)  $\sin 2x + \cos 2x$  (D)  $0.5 - 0.5 \cos 2x$

**Q.49** If  $u(t)$  is the unit step and  $\delta(t)$  is the unit impulse function, the inverse  $z$ -transform of  $F(z) = \frac{1}{z+1}$  for  $k > 0$  is

- (A)  $(-1)^k \delta(k)$  (B)  $\delta(k) - (-1)^k$   
 (C)  $(-1)^k u(k)$  (D)  $u(k) - (-1)^k$

**Q.50** Two magnetic poles revolve around a stationary armature carrying two coil ( $c_1 - c_1', c_2 - c_2'$ ) as shown in the figure. Consider the instant when the poles are in a position as shown. Identify the correct statement regarding the polarity of the induced emf at this instant in coil sides  $c_1$  and  $c_2$ .



- (A)  $\odot$  in  $c_1$ , no emf in  $c_2$  (B)  $\otimes$  in  $c_1$ , no emf in  $c_2$   
 (C)  $\odot$  in  $c_2$ , no emf in  $c_1$  (D)  $\otimes$  in  $c_2$ , no emf in  $c_1$

**Q.51** A 50 kW dc shunt is loaded to draw rated armature current at any given speed. When driven

- (i) at half the rated speed by armature voltage control and  
 (ii) at 1.5 times the rated speed by field control, the respective output powers delivered by the motor are approximately.  
 (A) 25 kW in (i) and 75 kW in (ii)  
 (B) 25 kW in (i) and 50 kW in (ii)

- (C) 50 kW in (i) and 75 kW in (ii)  
 (D) 50 kW in (i) and 50 kW in (ii)

**Q.52** In relation to DC machines, match the following and choose the correct combination

**List-I**

Performance Variables

P. Armature emf ( $E$ )Q. Developed torque ( $T$ )R. Developed power ( $P$ )**List-II**

Proportional to

1. Flux( $\phi$ ), speed ( $\omega$ ) and armature current ( $I_a$ )
2.  $\phi$  and  $\omega$  only
3.  $\phi$  and  $I_a$  only
4.  $I_a$  and  $\omega$  only
5.  $I_a$  only

**Codes:**

	P	Q	R
(A)	3	3	1
(B)	2	5	4
(C)	3	5	4
(D)	2	3	1



**Q.53** In relation to the synchronous machines, which one of the following statements is false ?

- (A) In salient pole machines, the direct-axis synchronous reactance is greater than the quadrature-axis synchronous reactance.  
 (B) The damper bars help the synchronous motor self start.  
 (C) Short circuit ratio is the ratio of the field current required to produce the rated voltage on open circuit to the rated armature current.  
 (D) The V-curve of a synchronous motor represents the variation in the armature current with field excitation, at a given output power.

**Q.54** Under no load condition, if the applied voltage to an induction motor is reduced from the rated voltage to half the rated value,

- (A) the speed decreases and the stator current increases  
 (B) both the speed and the stator current decrease

- (C) the speed and the stator current remain practically constant  
(D) there is negligible change in the speed but the stator current decreases

**Q.55** A three-phase cage induction motor is started by direct-on-line (DOL) switching at the rated voltage. If the starting current drawn is 6 times the full load current, and the full load slip is 4%, then ratio of the starting developed torque to the full load torque is approximately equal to

- (A) 0.24 (B) 1.44  
(C) 2.40 (D) 6.00

**Q.56** In a single phase induction motor driving a fan load, the reason for having a high resistance rotor is to achieve

- (A) low starting torque (B) quick acceleration  
(C) high efficiency (D) reduced size

**Q.57** Determine the correctness or otherwise of the following assertion[A] and the reason[R]

Assertion [A] : Under  $V/f$  control of induction motor, the maximum value of the developed torque remains constant over a wide range of speed in the sub-synchronous region.

Reason [R] : The magnetic flux is maintained almost constant at the rated value by keeping the ration  $V/f$  constant over the considered speed range.

- (A) Both [A] and [R] are true and [R] is the correct reason for [A]  
(B) Both [A] and [R] are true and but [R] is not the correct reason for [A]  
(C) Both [A] and [R] are false  
(D) [A] is true but [R] is false

**Q.58** The parameters of a transposed overhead transmission line are given as :

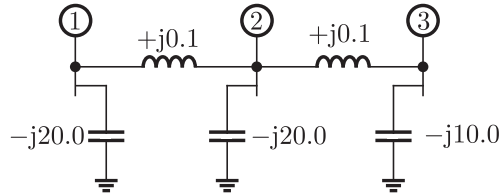
Self reactance  $X_S = 0.4\Omega/\text{km}$  and Mutual reactance  $X_m = 0.1\Omega/\text{km}$  The positive sequence reactance  $X_1$  and zero sequence reactance  $X_0$ , respectively in  $\Omega/\text{km}$  are

- (A) 0.3, 0.2 (B) 0.5, 0.2  
(C) 0.5, 0.6 (D) 0.3, 0.6

**Q.59** At an industrial sub-station with a 4 MW load, a capacitor of 2 MVAR is installed to maintain the load power factor at 0.97 lagging. If the capacitor goes out of service, the load power factor becomes

- (A) 0.85
- (B) 1.00
- (C) 0.80 lag
- (D) 0.90 lag

**Q.60** The network shown in the given figure has impedances in p.u. as indicated. The diagonal element  $Y_{22}$  of the bus admittance matrix  $Y_{BUS}$  of the network is

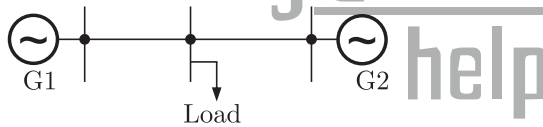


- (A)  $-j19.8$
- (B)  $+j20.0$
- (C)  $+j0.2$
- (D)  $-j19.95$

**Q.61** A load centre is at an equidistant from the two thermal generating stations  $G_1$  and  $G_2$  as shown in the figure. The fuel cost characteristic of the generating stations are given by

$$F_1 = a + bP_1 + cP_1^2 \text{ Rs/hour}$$

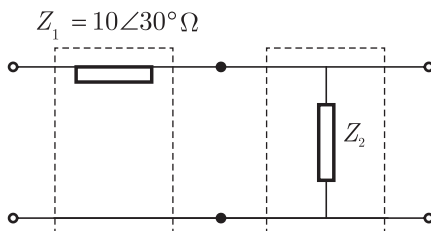
$$F_2 = a + bP_2 + 2cP_2^2 \text{ Rs/ hour}$$



Where  $P_1$  and  $P_2$  are the generation in MW of  $G_1$  and  $G_2$ , respectively. For most economic generation to meet 300 MW of load  $P_1$  and  $P_2$  respectively, are

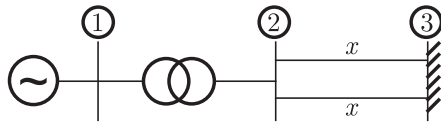
- (A) 150, 150
- (B) 100, 200
- (C) 200, 100
- (D) 175, 125

**Q.62** Two networks are connected in cascade as shown in the figure. With usual notations the equivalent  $A, B, C$  and  $D$  constants are obtained. Given that,  $C = 0.025 \angle 45^\circ$ , the value of  $Z_2$  is



- (A)  $10\angle 30^\circ \Omega$
- (B)  $40\angle -45^\circ \Omega$
- (C)  $1 \Omega$
- (D)  $0 \Omega$

**Q.63** A generator with constant 1.0 p.u. terminal voltage supplies power through a step-up transformer of 0.12 p.u. reactance and a double-circuit line to an infinite bus bar as shown in the figure. The infinite bus voltage is maintained at 1.0 p.u. Neglecting the resistances and susceptances of the system, the steady state stability power limit of the system is 6.25 p.u. If one of the double-circuit is tripped, then resulting steady state stability power limit in p.u. will be



- (A) 12.5 p.u.
- (B) 3.125 p.u.
- (C) 10.0 p.u.
- (D) 5.0 p.u.

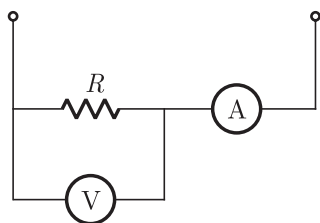
**Q.64** The simultaneous application of signals  $x(t)$  and  $y(t)$  to the horizontal and vertical plates, respectively, of an oscilloscope, produces a vertical figure-of-8 display. If P and Q are constants and  $x(t) = P \sin(4t + 30^\circ)$ , then  $y(t)$  is equal to

- (A)  $Q \sin(4t - 30^\circ)$
- (B)  $Q \sin(2t + 15^\circ)$
- (C)  $Q \sin(8t + 60^\circ)$
- (D)  $Q \sin(4t + 30^\circ)$

**Q.65** A DC ammeter has a resistance of  $0.1 \Omega$  and its current range is 0-100 A. If the range is to be extended to 0-500 A, then meter required the following shunt resistance

- (A)  $0.010 \Omega$
- (B)  $0.011 \Omega$
- (C)  $0.025 \Omega$
- (D)  $1.0 \Omega$

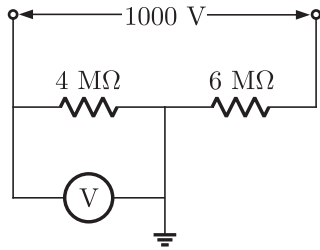
**Q.66** The set-up in the figure is used to measure resistance  $R$ . The ammeter and voltmeter resistances are  $0.01 \Omega$  and  $2000 \Omega$ , respectively. Their readings are 2 A and 180 V, respectively, giving a measured resistances of  $90 \Omega$ . The percentage error in the measurement is





- (A) 2.25% (B) 2.35%  
 (C) 4.5% (D) 4.71%

**Q.67** A 1000 V DC supply has two 1-core cables as its positive and negative leads : their insulation resistances to earth are  $4\text{ M}\Omega$  and  $6\text{ M}\Omega$ , respectively, as shown in the figure. A voltmeter with resistance  $50\text{ k}\Omega$  is used to measure the insulation of the cable. When connected between the positive core and earth, then voltmeter reads

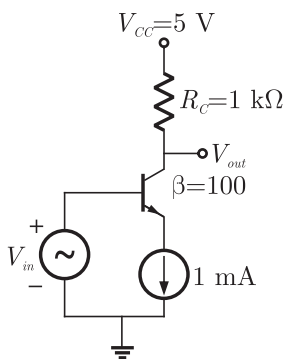


- (A) 8 V (B) 16 V  
 (C) 24 V (D) 40 V

**Q.68** Two wattmeters, which are connected to measure the total power on a three-phase system supplying a balanced load, read  $10.5\text{ kW}$  and  $-2.5\text{ kW}$ , respectively. The total power and the power factor, respectively, are

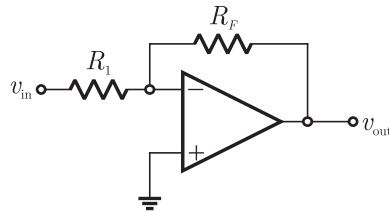
- (A)  $13.0\text{ kW}$ ,  $0.334$  (B)  $13.0\text{ kW}$ ,  $0.684$   
 (C)  $8.0\text{ kW}$ ,  $0.52$  (D)  $8.0\text{ kW}$ ,  $0.334$

**Q.69** The common emitter amplifier shown in the figure is biased using a  $1\text{ mA}$  ideal current source. The approximate base current value is



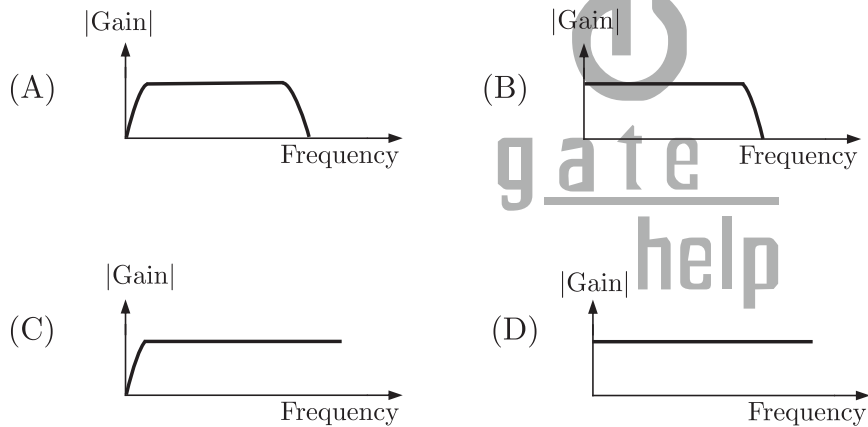
- (A)  $0\text{ }\mu\text{A}$  (B)  $10\text{ }\mu\text{A}$   
 (C)  $100\text{ }\mu\text{A}$  (D)  $1000\text{ }\mu\text{A}$

**Q.70** Consider the inverting amplifier, using an ideal operational amplifier shown in the figure. The designer wishes to realize the input resistance seen by the small-signal source to be as large as possible, while keeping the voltage gain between  $-10$  and  $-25$ . The upper limit on  $R_F$  is  $1\text{ M}\Omega$ . The value of  $R_I$  should be

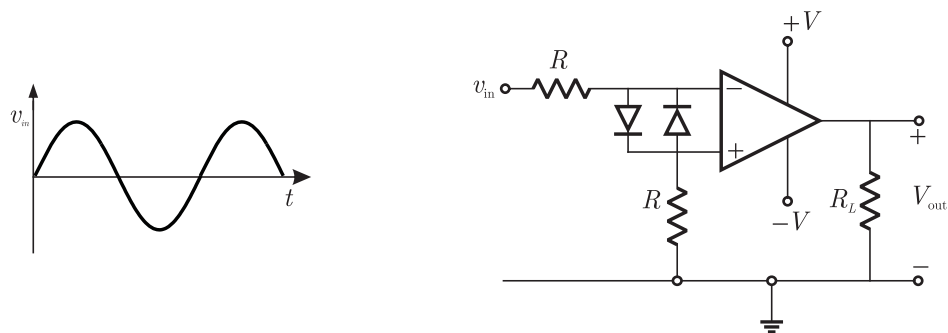


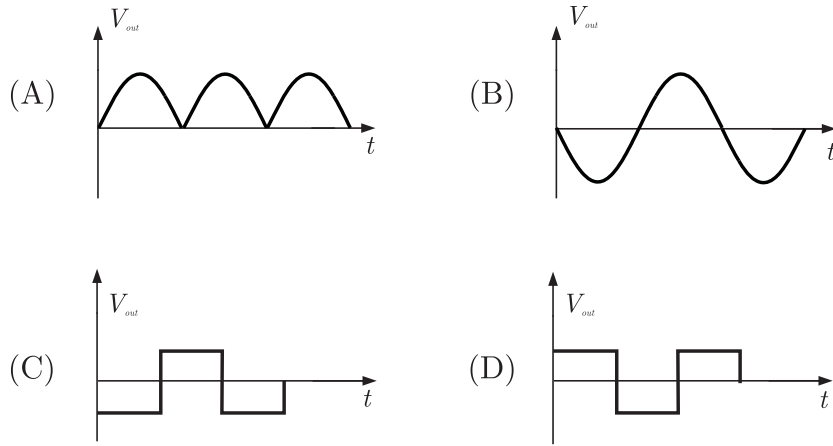
- (A) Infinity  
(B)  $1\text{ M}\Omega$   
(C)  $100\text{ k}\Omega$   
(D)  $40\text{ k}\Omega$

**Q.71** The typical frequency response of a two-stage direct coupled voltage amplifier is as shown in figure

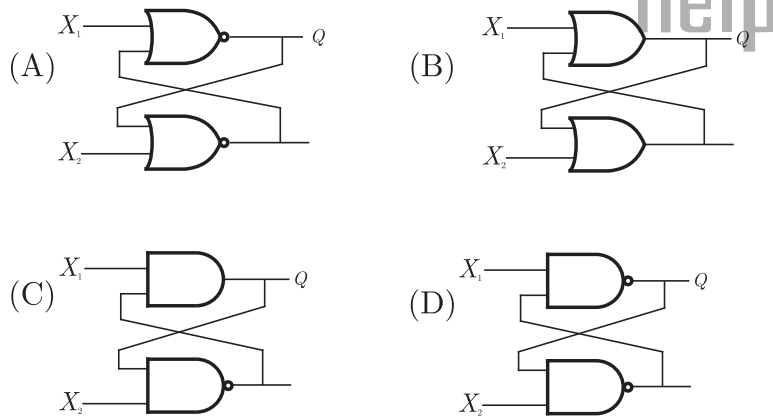
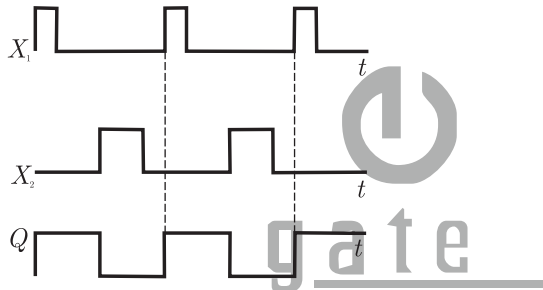


**Q.72** In the given figure, if the input is a sinusoidal signal, the output will appear as shown

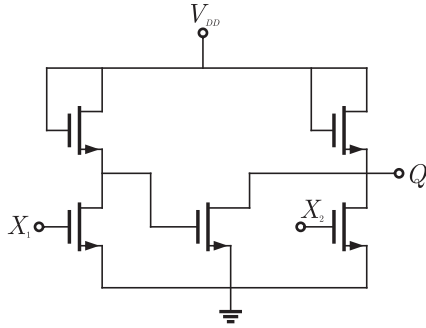




**Q.73** Select the circuit which will produce the given output  $Q$  for the input signals  $X_1$  and  $X_2$  given in the figure

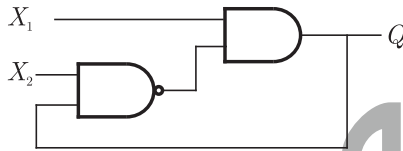


**Q.74** If  $X_1$  and  $X_2$  are the inputs to the circuit shown in the figure, the output  $Q$  is



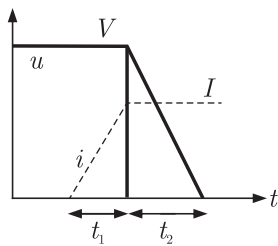
- (A)  $\overline{X_1 + X_2}$
- (B)  $\overline{X_1 \cdot X_2}$
- (C)  $\overline{X_1} \cdot X_2$
- (D)  $X_1 \cdot \overline{X_2}$

**Q.75** In the figure, as long as  $X_1 = 1$  and  $X_2 = 1$ , the output  $Q$  remains



- (A) at 1
- (B) at 0
- (C) at its initial value
- (D) unstable

**Q.76** The figure shows the voltage across a power semiconductor device and the current through the device during a switching transitions. If the transition a turn ON transition or a turn OFF transition ? What is the energy lost during the transition?



- (A) Turn ON,  $\frac{VI}{2}(t_1 + t_2)$
- (B) Turn OFF,  $VI(t_1 + t_2)$
- (C) Turn ON,  $VI(t_1 + t_2)$
- (D) Turn OFF,  $\frac{VI}{2}(t_1 + t_2)$

**Q.77** An electronics switch S is required to block voltage of either polarity during its OFF state as shown in the figure (a). This switch is required to conduct in only one direction its ON state as shown in the figure (b)

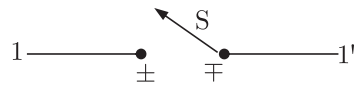
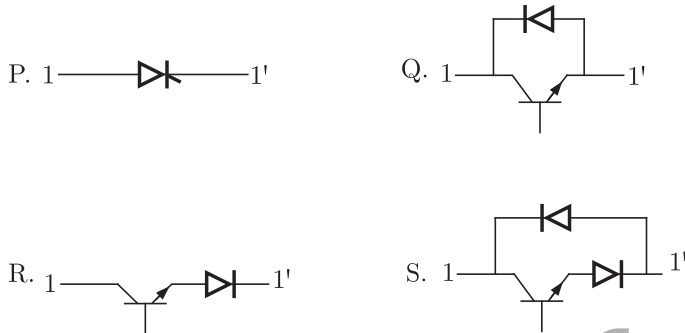


fig (a)



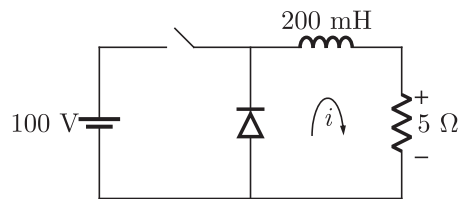
fig (b)

Which of the following are valid realizations of the switch S?



- (A) Only P
- (B) P and Q
- (C) P and R
- (D) R and S

**Q.78** The given figure shows a step-down chopper switched at 1 kHz with a duty ratio  $D = 0.5$ . The peak-peak ripple in the load current is close to

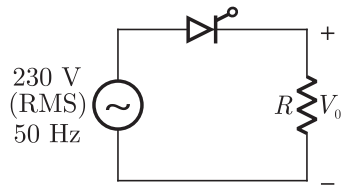


- (A) 10 A
- (B) 0.5 A
- (C) 0.125 A
- (D) 0.25 A

**Q.79** An electric motor, developing a starting torque of 15 Nm, starts with a load torque of 7 Nm on its shaft. If the acceleration at start is  $2 \text{ rad/sec}^2$ , the moment of inertia of the system must be (neglecting viscous and coulomb friction)

- (A)  $0.25 \text{ kg-m}^2$
- (B)  $0.25 \text{ Nm}^2$
- (C)  $4 \text{ kg-m}^2$
- (D)  $4 \text{ Nm}^2$

**Q.80** Consider a phase-controlled converter shown in the figure. The thyristor is fired at an angle  $\alpha$  in every positive half cycle of the input voltage. If the peak value of the instantaneous output voltage equals 230 V, the firing angle  $\alpha$  is close to



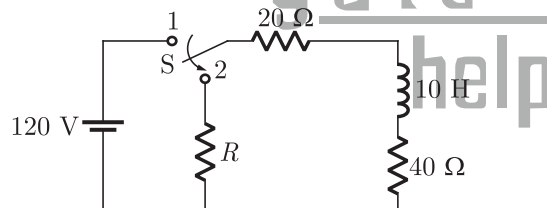
- (A)  $45^\circ$  (B)  $135^\circ$   
 (C)  $90^\circ$  (D)  $83.6^\circ$

**Linked Answer Questions : Q. 81a to Q.85b Carry Two Marks Each**

**Statement for Linked Answer Questions 81a and 81b**

A coil of inductance 10 H and resistance  $40 \Omega$  is connected as shown in the figure. After the switch S has been in contact with point 1 for a very long time, it is moved to point 2 at,  $t = 0$ .

**Q.81a** If, at  $t = 0^+$ , the voltage across the coil is 120 V, the value of resistance  $R$  is



- (A)  $0 \Omega$  (B)  $20 \Omega$   
 (C)  $40 \Omega$  (D)  $60 \Omega$

**Q.81b** For the value as obtained in (a), the time taken for 95% of the stored energy to be dissipated is close to

- (A) 0.10 sec (B) 0.15 sec  
 (C) 0.50 sec (D) 1.0 sec

**Statement for Linked Answer Questions 82a and 82b**

A state variable system  $\dot{\mathbf{X}}(t) = \begin{bmatrix} 0 & 1 \\ 0 & -3 \end{bmatrix} \mathbf{X}(t) + \begin{bmatrix} 1 \\ 0 \end{bmatrix} \mathbf{u}(t)$  with the initial condition  $\mathbf{X}(0) = [-1, 3]^T$  and the unit step input  $\mathbf{u}(t)$  has

**Q.82a** The state transition matrix

- (A)  $\begin{bmatrix} 1 & \frac{1}{3}(1 - e^{-3t}) \\ 0 & e^{-3t} \end{bmatrix}$       (B)  $\begin{bmatrix} 1 & \frac{1}{3}(e^{-t} - e^{-3t}) \\ 0 & e^{-t} \end{bmatrix}$
- (C)  $\begin{bmatrix} 1 & \frac{1}{3}(e^{3-t} - e^{-3t}) \\ 0 & e^{-3t} \end{bmatrix}$       (D)  $\begin{bmatrix} 1 & (1 - e^{-t}) \\ 0 & e^{-t} \end{bmatrix}$

**Q.82b** The state transition equation

- (A)  $\mathbf{X}(t) = \begin{bmatrix} t - e^{-t} \\ e^{-t} \end{bmatrix}$       (B)  $\mathbf{X}(t) = \begin{bmatrix} 1 - e^{-t} \\ 3e^{-3t} \end{bmatrix}$
- (C)  $\mathbf{X}(t) = \begin{bmatrix} t - e^{3t} \\ 3e^{-3t} \end{bmatrix}$       (D)  $\mathbf{X}(t) = \begin{bmatrix} t - e^{-3t} \\ e^{-t} \end{bmatrix}$

**Statement for Linked Answer Questions 83a and 83b.**

A 1000 kVA, 6.6 kV, 3-phase star connected cylindrical pole synchronous generator has a synchronous reactance of  $20 \Omega$ . Neglect the armature resistance and consider operation at full load and unity power factor.

**Q.83a** The induced emf(line-to-line) is close to

- (A) 5.5 kV      (B) 7.2 kV
- (C) 9.6 kV      (D) 12.5 kV

**Q.83b** The power(or torque) angle is close to

- (A)  $13.9^\circ$       (B)  $18.3^\circ$
- (C)  $24.6^\circ$       (D)  $33.0^\circ$

**Statement for Linked Answer Questions 84a and 84b**

At a 220 kV substation of a power system, it is given that the three-phase fault level is 4000 MVA and single-line to ground fault level is 5000 MVA Neglecting the resistance and the shunt susceptances of the system.

**Q.84a** The positive sequence driving point reactance at the bus is

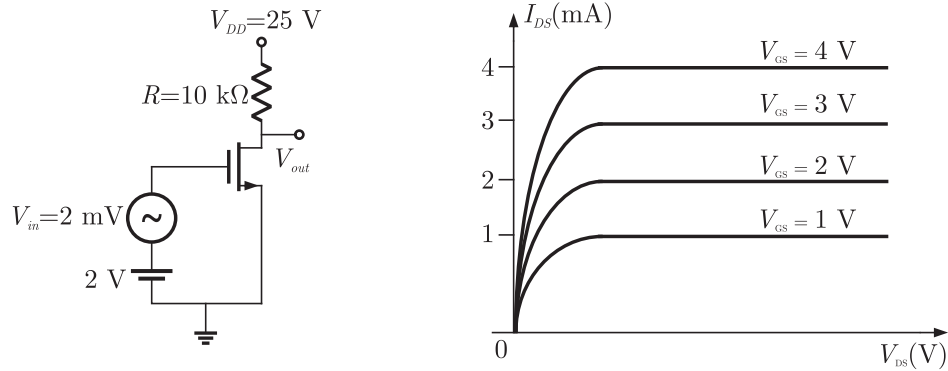
- (A)  $2.5 \Omega$       (B)  $4.033 \Omega$
- (C)  $5.5 \Omega$       (D)  $12.1 \Omega$

**Q.84b** The zero sequence driving point reactance at the bus is

- (A)  $2.2 \Omega$       (B)  $4.84 \Omega$
- (C)  $18.18 \Omega$       (D)  $22.72 \Omega$

**Statement for Linked Answer Questions 85a and 85b**

Assume that the threshold voltage of the N-channel MOSFET shown in figure is  $+ 0.75$  V. The output characteristics of the MOSFET are also shown



**Q.85a** The transconductance of the MOSFET is

- (A) 0.75 ms (B) 1 ms  
(C) 2 ms (D) 10 ms

**Q.85b** The voltage gain of the amplifier is

- (A) +5 (B) -7.5  
(C) +10 (D) -10

gate  
\*\*\*\*\*  
help